



CALCULATION PACKAGE

August 29, 2024

LNL Builds

27xx 62nd Ave
Mercer Island, WA

MULHERN & KULP STRUCTURAL ENGINEERING, INC.

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Signature, Seal & Date

Beam & Header Calculations

Beam Description:

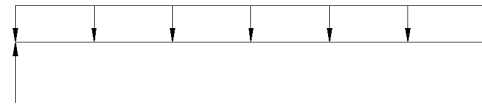
B1 - ROOF - PRIMARY BDR - HDR @ DECK

Parameters:

L = 3.33 ft

W = 0.620 kl f

P = - k



Analysis:

$R_{max} = 1.03$ K $V_d =$ K < $V_{all} = 3.50$ K Adequate

$M_{max} = 0.86$ k-ft < $M_{all} = 3.40$ k-ft Adequate

$\Delta_{tl} = 0.010$ in. L/ 999+ < L/240 Adequate

4x8 DFL #2

Beam Description:

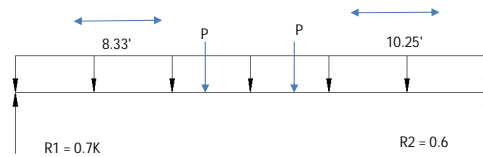
B2 - ROOF - BM OVER PRIMARY BATH

Parameters:

L = 20.67 ft

W = - kl f

P = 0.6 k



Analysis:

$R_{max} = 0.70$ K $V_d =$ K < $V_{all} = 9.10$ K Adequate

$M_{max} = 6.20$ k-ft < $M_{all} = 20.50$ k-ft Adequate

$\Delta_{tl} = 0.510$ in. L/ 486 < L/240 Adequate

3-1/2"x11-7/8" LVL

Beam Description:

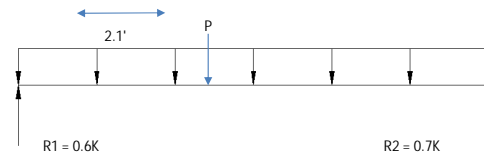
B3 - ROOF - HDR AT PRIMARY BATH

Parameters:

L = 3.00 ft

W = 0.240 kl f

P = 0.7 k



Analysis:

$R_{max} = 0.90$ K $V_d =$ K < $V_{all} = 3.50$ K Adequate

$M_{max} = 0.70$ k-ft < $M_{all} = 3.40$ k-ft Adequate

$\Delta_{tl} = 0.006$ in. L/ 999+ < L/240 Adequate

4x8 DFL #2

Beam & Header Calculations

Beam Description:

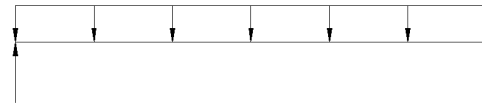
B4 - ROOF - BM OVER BATHROOM

Parameters:

L = 4.50 ft

W = 0.280 kl f

P = - k



Analysis:

$R_{max} = 0.63$ K $V_d =$ K $< V_{all} = 4.50$ K Adequate

$M_{max} = 0.71$ k-ft $< M_{all} = 10.20$ k-ft Adequate

$\Delta_{tl} = 0.006$ in. $L/999+$ $< L/240$ Adequate

1-3/4"x11-7/8" LVL

Beam Description:

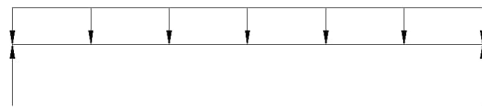
B5 - ROOF - INT HDR AT PRIMARY BEDROOM

Parameters:

L = 2.90 ft

W = 0.550 kl f

P = - k



Analysis:

$R_{max} = 0.80$ K $V_d =$ K $< V_{all} = 3.50$ K Adequate

$M_{max} = 0.58$ k-ft $< M_{all} = 3.40$ k-ft Adequate

$\Delta_{tl} = 0.005$ in. $L/999+$ $< L/240$ Adequate

4x8 DFL #2

Beam Description:

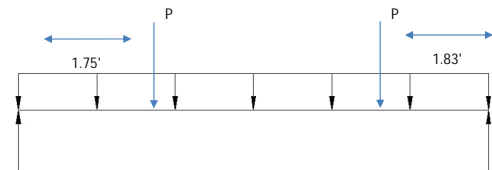
B6 - ROOF - BM AT STAIRS

Parameters:

L = 7.75 ft

W = 0.380 kl f

P = 0.3 k



Analysis:

$R_{max} = 1.80$ K $V_d =$ K $< V_{all} = 9.10$ K Adequate

$M_{max} = 4.02$ k-ft $< M_{all} = 20.50$ k-ft Adequate

$\Delta_{tl} = 0.047$ in. $L/999+$ $< L/240$ Adequate

3-1/2"x11-7/8" LVL

Beam & Header Calculations

Beam Description:

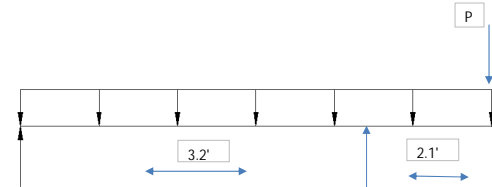
B7 - ROOF - STRUCT. FASCIA @ BEDROOM EAVE

Parameters:

L = 4.50 ft

W = 0.065 kl f

P = 0.3 k



Analysis:

$R_{max} = 0.80$ K $V_d =$ K $< V_{all} = 4.50$ K Adequate

$M_{max} = -0.80$ k-ft $< M_{all} = -10.20$ k-ft Adequate

$\Delta_{tl} = 0.010$ in. $L/999+$ $< L/240$ Adequate

1-3/4"x11-7/8" LVL

Beam Description:

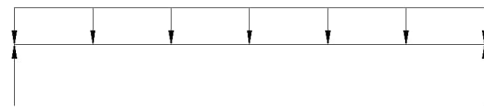
B8 - ROOF - FLUSH HDR AT BEDROOM

Parameters:

L = 4.50 ft

W = 0.290 kl f

P = - k



Analysis:

$R_{max} = 0.70$ K $V_d =$ K $< V_{all} = 9.10$ K Adequate

$M_{max} = 0.70$ k-ft $< M_{all} = 20.50$ k-ft Adequate

$\Delta_{tl} = 0.003$ in. $L/999+$ $< L/240$ Adequate

3-1/2"x11-7/8" LVL

Beam Description:

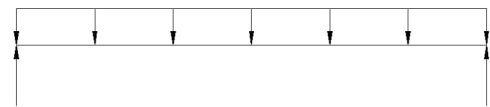
B9 - UPPER FLOOR - HDR AT GARAGE REAR DOOR

Parameters:

L = 3.33 ft

W = 0.770 kl f

P = - k



Analysis:

$R_{max} = 1.28$ K $V_d =$ K $< V_{all} = 3.00$ K Adequate

$M_{max} = 1.10$ k-ft $< M_{all} = 3.00$ k-ft Adequate

$\Delta_{tl} = 0.012$ in. $L/999+$ $< L/240$ Adequate

4x8 DFL #2

Beam & Header Calculations

Beam Description:

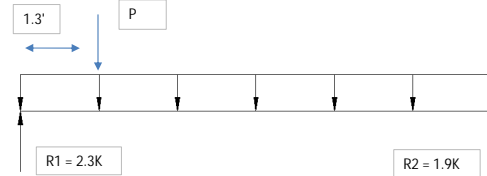
B10 - UPPER FLOOR - FLUSH BM AT REAR GARAGE EXIT

Parameters:

L = 4.50 ft

W = 0.750 kl f

P = 0.8 k



Analysis:

$R_{max} = 2.30$ K $V_d =$ K $< V_{all} = 12.80$ K Adequate

$M_{max} = 2.60$ k-ft $< M_{all} = 43.50$ k-ft Adequate

$\Delta_{tl} = 0.003$ in. $L/999+$ $< L/240$ Adequate

3-1/2"x18" GLB

Beam Description:

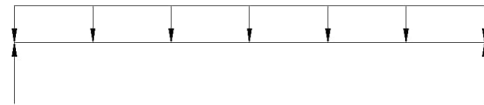
B11 - UPPER FLOOR - BM AT REAR PATIO COVER

Parameters:

L = 3.70 ft

W = 0.155 kl f

P = - k



Analysis:

$R_{max} = 0.21$ K $V_d =$ K $< V_{all} = 4.50$ K Adequate

$M_{max} = 0.20$ k-ft $< M_{all} = 5.20$ k-ft Adequate

$\Delta_{tl} = 0.001$ in. $L/999+$ $< L/240$ Adequate

4x10 DFL #2

Beam Description:

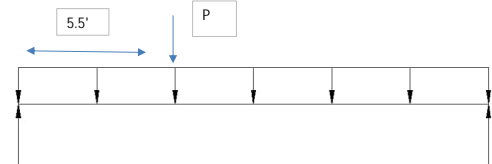
B12 - UPPER FLOOR - BM AT REAR PATIO COVER

Parameters:

L = 19.00 ft

W = 0.070 kl f

P = 0.2 k



Analysis:

$R_{max} = 0.81$ K $V_d =$ K $< V_{all} = 7.50$ K Adequate

$M_{max} = 0.73$ k-ft $< M_{all} = 14.80$ k-ft Adequate

$\Delta_{tl} = 0.425$ in. $L/536$ $< L/240$ Adequate

3-1/2"x10-1/2" GLB

Beam & Header Calculations

Beam Description:

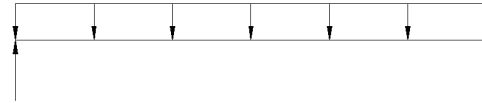
B13 - UPPER FLOOR - BM AT REAR PATIO COVER

Parameters:

L = 17.20 ft

W = 0.102 kl f

P = - k



Analysis:

$R_{max} = 0.90$ K $V_d =$ K $< V_{all} = 7.50$ K Adequate

$M_{max} = 3.80$ k-ft $< M_{all} = 14.80$ k-ft Adequate

$\Delta_{tl} = 0.330$ in. L/ 625 $< L/240$ Adequate

3-1/2"x10-1/2" GLB

Beam Description:

B14 - UPPER FLOOR - REAR FLUSH BM @ LIVING ROOM

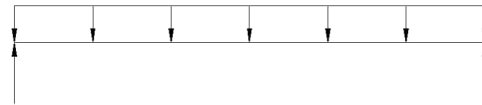
Parameters:

SEE ENERCALC

L = ft

W = kl f

P = k



Analysis:

$R_{max} =$ K $V_d =$ K $< V_{all} =$ K Adequate

$M_{max} =$ k-ft $< M_{all} =$ k-ft Adequate

$\Delta_{tl} =$ in. L/ $< L/240$ Adequate

3-1/2"x18" GLB

Beam Description:

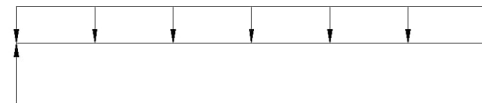
B15 - UPPER FLOOR - REAR FLUSH BM @ LIVING ROOM

Parameters:

L = 2.75 ft

W = 0.580 kl f

P = - k



Analysis:

$R_{max} = 0.80$ K $V_d =$ K $< V_{all} = 3.90$ K Adequate

$M_{max} = 0.55$ k-ft $< M_{all} = 2.00$ k-ft Adequate

$\Delta_{tl} = 0.008$ in. L/ 999+ $< L/240$ Adequate

6x6 DFL #2

Beam & Header Calculations

Beam Description:

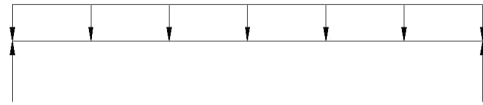
B16 - UPPER FLOOR - BM AT FLUSH ENTRY SHOWER

Parameters:

L = 12.50 ft

W = 0.460 kl f

P = - k



Analysis:

$R_{max} = 2.90$ K $V_d =$ [] K $< V_{all} = 11.10$ K Adequate

$M_{max} = 9.00$ k-ft $< M_{all} = 37.80$ k-ft Adequate

$\Delta_{tl} = 0.083$ in. $L/999+$ $< L/240$ Adequate

3-1/2"x18" GLB

Beam Description:

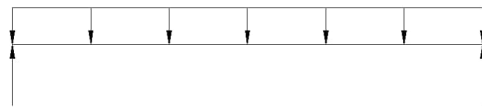
B17 - N/A

Parameters:

L = [] ft

W = [] kl f

P = [] k



Analysis:

$R_{max} =$ [] K $V_d =$ [] K $< V_{all} =$ [] K Adequate

$M_{max} =$ [] k-ft $< M_{all} =$ [] k-ft Adequate

$\Delta_{tl} =$ [] in. $L/$ [] $< L/240$ Adequate

Beam Description:

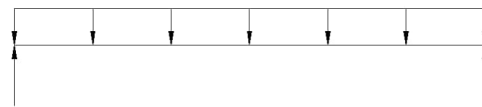
B18 - UPPER FLOOR - DECK REAR BEAM

Parameters:

L = 16.10 ft

W = 0.130 kl f

P = - k



Analysis:

$R_{max} = 1.05$ K $V_d =$ [] K $< V_{all} = 3.90$ K Adequate

$M_{max} = 4.21$ k-ft $< M_{all} = 4.50$ k-ft Adequate

$\Delta_{tl} = 0.530$ in. $L/363$ $< L/240$ Adequate

4x10 DFL #2

Beam & Header Calculations

Beam Description:

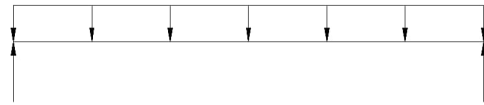
B19 - UPPER FLOOR - DECK REAR BEAM

Parameters:

L = 6.10 ft

W = 0.250 kl f

P = - k



Analysis:

$R_{max} = 0.76$ K $V_d =$ [] K $< V_{all} = 3.90$ K Adequate

$M_{max} = 1.16$ k-ft $< M_{all} = 4.50$ k-ft Adequate

$\Delta_{tl} = 0.021$ in. $L/999+$ $< L/240$ Adequate

4x10 DFL #2

Beam Description:

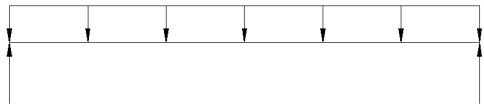
B20 - UPPER FLOOR - REAR BEAM UNDER B.W.A. @ DECK

Parameters:

L = 16.00 ft

W = 1.020 kl f

P = - k



Analysis:

$R_{max} = 8.16$ K $V_d =$ [] K $< V_{all} = 17.50$ K Adequate

$M_{max} = 32.64$ k-ft $< M_{all} = 59.40$ k-ft Adequate

$\Delta_{tl} = 0.313$ in. $L/614$ $< L/240$ Adequate

5-1/2"x18" GLB

Beam Description:

B21 - UPPER FLOOR - CANTD BM AT REAR DECK

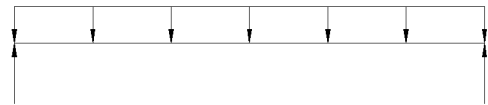
Parameters:

SEE ENERCALC

L = [] ft

W = [] kl f

P = [] k



Analysis:

$R_{max} =$ [] K $V_d =$ [] K $< V_{all} =$ [] K Adequate

$M_{max} =$ [] k-ft $< M_{all} =$ [] k-ft Adequate

$\Delta_{tl} =$ [] in. $L/$ [] $< L/240$ Adequate

W14x30

Beam & Header Calculations

Beam Description:

B22 - UPPER FLOOR - BM ABOVE KITCHEN

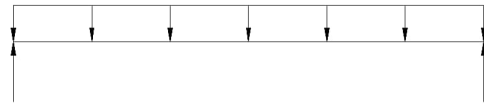
Parameters:

SEE ENERCALC

L = ft

W = kl f

P = k



Analysis:

$R_{max} =$ K $V_d =$ K $< V_{all} =$ K Adequate

$M_{max} =$ k-ft $< M_{all} =$ k-ft Adequate

$\Delta_{tl} =$ in. $L/$ $< L/240$ Adequate

5-1/2"x18" GLB

Beam Description:

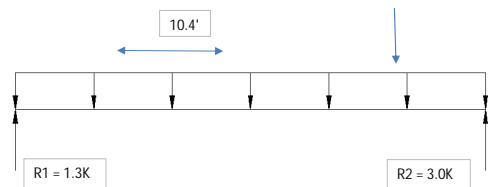
B23 - UPPER FLOOR - BM AT STAIRS

Parameters:

L = ft

W = kl f

P = k



Analysis:

$R_{max} =$ K $V_d =$ K $< V_{all} =$ K Adequate

$M_{max} =$ k-ft $< M_{all} =$ k-ft Adequate

$\Delta_{tl} =$ in. $L/$ $< L/240$ Adequate

3-1/2"x18" GLB

Beam Description:

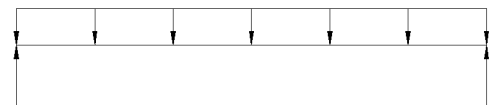
B24 - UPPER FLOOR - BM AT STAIRS

Parameters:

L = ft

W = kl f

P = k



Analysis:

$R_{max} =$ K $V_d =$ K $< V_{all} =$ K Adequate

$M_{max} =$ k-ft $< M_{all} =$ k-ft Adequate

$\Delta_{tl} =$ in. $L/$ $< L/240$ Adequate

3-1/2"x18" GLB

Beam & Header Calculations

Beam Description:

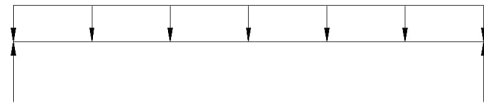
B25 - UPPER FLOOR - HDR AT FRONT COVERED PORCH

Parameters:

L = 4.33 ft

W = 0.480 kl f

P = - k



Analysis:

$R_{max} = 1.00$ K $V_d =$ K < $V_{all} = 3.00$ K Adequate

$M_{max} = 1.12$ k-ft < $M_{all} = 3.00$ k-ft Adequate

$\Delta_{tl} = 0.021$ in. $L/999+$ < $L/240$ Adequate

6x6 DFL #2

Beam Description:

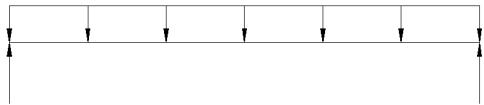
B26 - UPPER FLOOR - EDGE BM @ B.W.A @ FRONT PORCH

Parameters:

L = 16.00 ft

W = 0.500 kl f

P = - k



Analysis:

$R_{max} = 4.00$ K $V_d =$ K < $V_{all} = 11.10$ K Adequate

$M_{max} = 16.00$ k-ft < $M_{all} = 37.80$ k-ft Adequate

$\Delta_{tl} = 0.241$ in. $L/797$ < $L/240$ Adequate

3-1/2"x18" GLB

Beam Description:

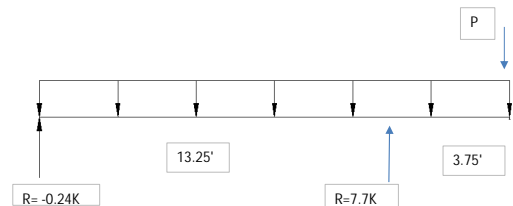
B27 - UPPER FLOOR - CANT'D BM @ FRONT PORCH

Parameters:

L = 17.00 ft

W = 0.170 kl f

P = 4.5 k



Analysis:

$R_{max} = 7.65$ K $V_d =$ K < $V_{all} = 12.80$ K Adequate

$M_{max} = -18.07$ k-ft < $M_{all} = -33.50$ k-ft Adequate

$\Delta_{tl} = 0.181$ in. $2L/497$ < $L/240$ Adequate

3-1/2"x18" GLB

Beam & Header Calculations

Beam Description:

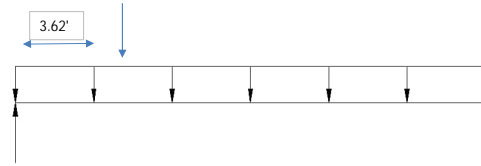
B28 - UPPER FLOOR - GARAGE HDR

Parameters:

L = 16.33 ft

W = 0.810 kl f

P = 1.4 k



Analysis:

$R_{max} = 7.70$ K $V_d =$ [] K $< V_{all} = 16.00$ K [X] Adequate

$M_{max} = 31.04$ k-ft $< M_{all} = 49.90$ k-ft [X] Adequate

$\Delta_{tl} = 0.402$ in. $L/487 < L/240$ [X] Adequate

5-1/2"x16" GLB

Beam Description:

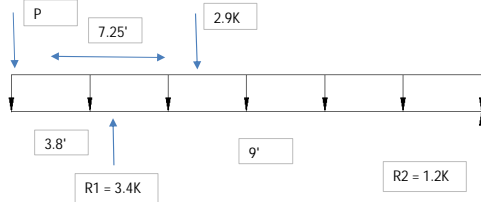
B29 - UPPER FLOOR - CANT'D BM AT REAR PATIO

Parameters:

L = 20.10 ft

W = 0.155 kl f

P = 0.6 k



Analysis:

$R_{max} = 2.40$ K $V_d =$ [] K $< V_{all} = 11.10$ K [X] Adequate

$M_{max} = 4.92$ k-ft $< M_{all} = 37.80$ k-ft [X] Adequate

$\Delta_{tl} = 0.019$ in. $L/999+ < L/240$ [X] Adequate

3-1/2"x18" GLB

Beam Description:

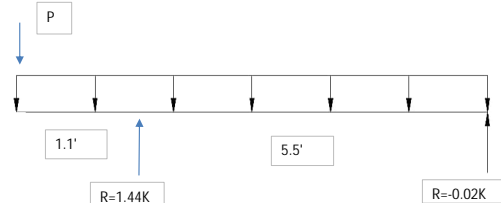
B30 - UPPER FLOOR - CANT'D BM AT REAR DECK

Parameters:

L = 6.60 ft

W = 0.047 kl f

P = 1.1 k



Analysis:

$R_{max} = 1.44$ K $V_d =$ [] K $< V_{all} = 3.90$ K [X] Adequate

$M_{max} = -1.18$ k-ft $< M_{all} = -4.50$ k-ft [X] Adequate

$\Delta_{tl} = 0.012$ in. $2L/999+ < L/240$ [X] Adequate

3-1/2"x18" GLB



Beam & Header Calculations

Beam Description:

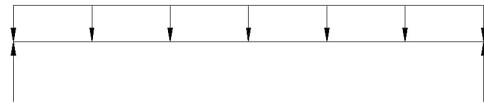
B31 - MAIN FLOOR - TYP CRAWL SPACE BEAM

Parameters:

L = 6.50 ft

W = 0.744 kl f

P = - k



Analysis:

$R_{max} = 2.40$ K $V_d =$ K $< V_{all} = 3.90$ K Adequate

$M_{max} = 3.90$ k-ft $< M_{all} = 4.50$ k-ft Adequate

$\Delta_{tl} = 0.081$ in. $L/964 < L/240$ Adequate

4x10 DFL #2

Beam Description:

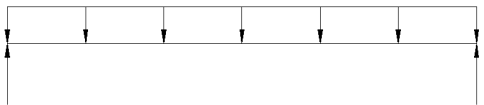
B32 - CRAWL SPACE BM

Parameters:

L = 7.60 ft

W = 0.550 kl f

P = - k



Analysis:

$R_{max} = 2.10$ K $V_d =$ K $< V_{all} = 3.90$ K Adequate

$M_{max} = 4.00$ k-ft $< M_{all} = 4.50$ k-ft Adequate

$\Delta_{tl} = 0.112$ in. $L/816 < L/240$ Adequate

4x10 DFL #2

Beam Description:

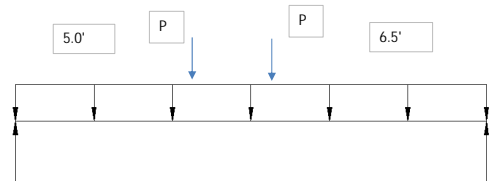
B33 - ROOF - BM AST SKYLIGHT BY STAIRS

Parameters:

L = 14.30 ft

W = - kl f

P = 0.2 k



Analysis:

$R_{max} = 0.23$ K $V_d =$ K $< V_{all} = 4.50$ K Adequate

$M_{max} = 1.40$ k-ft $< M_{all} = 10.20$ k-ft Adequate

$\Delta_{tl} = 0.111$ in. $2L/999+ < L/240$ Adequate

1-3/4"x11-7/8" LVL



Beam & Header Calculations

Beam Description:

B34 - UPPER FLOOR - BM ABOVE KITCHEN

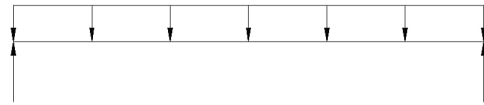
Parameters:

SEE ENERCALC

L = ft

W = kl f

P = k



Analysis:

$R_{max} =$ K $V_d =$ K $< V_{all} =$ K Adequate

$M_{max} =$ k-ft $< M_{all} =$ k-ft Adequate

$\Delta_{tl} =$ in. $L/$ $< L/240$ Adequate

3-1/2"x18" GLB

Beam Description:

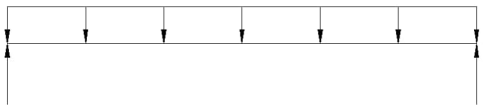
B35 - UPPER FLOOR - LOW ROOF RAFTERS

Parameters:

L = ft

W = kl f

P = k



Analysis:

$R_{max} =$ K $V_d =$ K $< V_{all} =$ K Adequate

$M_{max} =$ k-ft $< M_{all} =$ k-ft Adequate

$\Delta_{tl} =$ in. $L/$ $< L/240$ Adequate

2x10 HF #2

Beam Description:

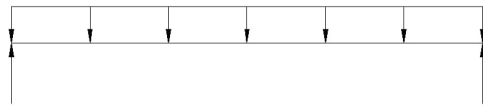
B36 - UPPER FLOOR - DECK JOIST

Parameters:

L = ft

W = kl f

P = k



Analysis:

$R_{max} =$ K $V_d =$ K $< V_{all} =$ K Adequate

$M_{max} =$ k-ft $< M_{all} =$ k-ft Adequate

$\Delta_{tl} =$ in. $2L/$ $< L/240$ Adequate

2x10 HF #2 @ 16" o.c.

Beam & Header Calculations

Beam Description:

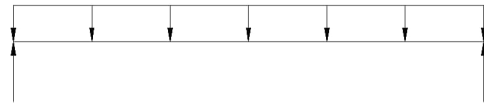
B37 - ROOF - CONT. FASCIA

Parameters:

L = 22.00 ft

W = 0.027 kl f

P = - k



Analysis:

$R_{max} = 0.28$ K $V_d =$ $V_d < V_{all} = 4.50$ K Adequate

$M_{max} = 1.42$ k-ft $M_{max} < M_{all} = 10.20$ k-ft Adequate

$\Delta_{tl} = 0.231$ in. $L/999+ < L/240$ Adequate

1-3/4"x11-7/8" LVL

Beam Description:

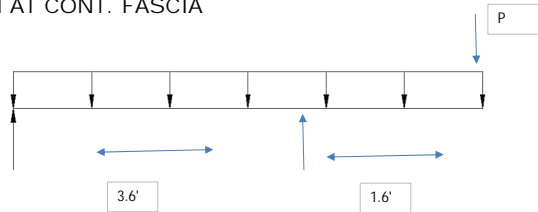
B38 - ROOF - CANTB BM AT CONT. FASCIA

Parameters:

L = 5.20 ft

W = 0.543 kl f

P = 0.6 k



Analysis:

$R_{max} = 2.91$ K $V_d =$ $V_d < V_{all} = 10.90$ K Adequate

$M_{max} = -1.66$ k-ft $M_{max} < M_{all} = -19.70$ k-ft Adequate

$\Delta_{tl} = 0.005$ in. $2L/999+ < L/240$ Adequate

3-1/2"x11-7/8" LVL

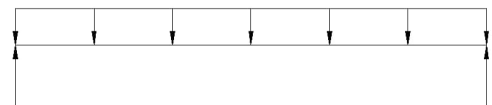
Beam Description:

Parameters:

L = 4.50 ft

W = 0.140 kl f

P = - k



Analysis:

$R_{max} = 0.32$ K $V_d =$ $V_d < V_{all} = 1.40$ K Adequate

$M_{max} = 0.35$ k-ft $M_{max} < M_{all} = 1.90$ k-ft Adequate

$\Delta_{tl} = 0.010$ in. $2L/999+ < L/240$ Adequate

2x10 HF #2 @ 16" o.c.



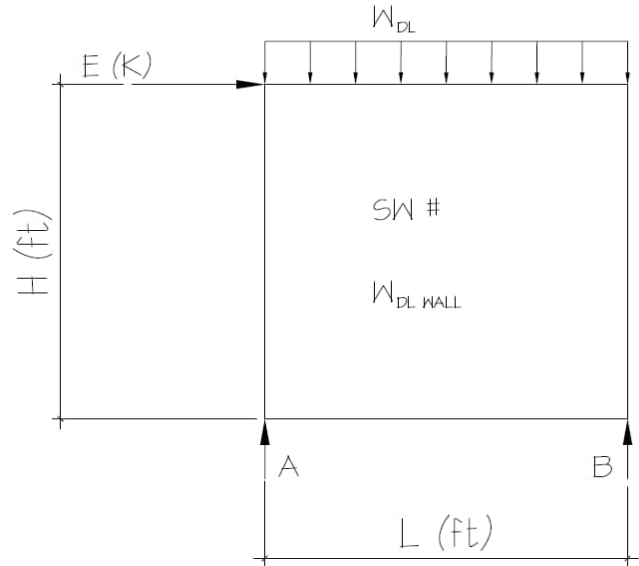
Overstrength Calculations

Wall Description/SW #:

201

Parameters:

L = 10.3 ft
 H = 9.8 ft
 E = 0.80 k
 W_{DLWall} = 0.10 klf
 W_{DL} = 0.030 klf
 Ω₀ = 2.5 (ASCE TABLE 12.2.1 FOOTNOTE)
 SDS = 1.122



analysis:

E (unfactored) = 1.14
 E_{mh} = Ω₀ * E = 2.86 K E_v = 0.2 * SDS * DL = 0.300 K
 E_m = E_{mh} + E_v = 3.158 K
 E_m = E_{mh} - E_v = 2.557 K

E_m (max) = ΣM_A = 0 = 3.16(9.8) + 0.13(10.3)(5.15) - R_b(10.3) R_B = 0.7DL + 3.0E
 Ra = 0.7DL - 3.0E
 E_m (min) = ΣM_A = 0 = 2.56(9.8) + 0.13(10.3)(5.15) - R_b(10.3) R_B = 0.7DL + 2.4E
 Ra = 0.7DL - 2.4E

check beams for axial forces shown using load combos per section 12.4.3.1 (asd)

allowable stress permitted to be increased by 1.2

see following beam calcs for load application



Overstrength Calculations

Wall Description/SW #:

203

Parameters:

L = 11.8 ft

H = 9.6 ft

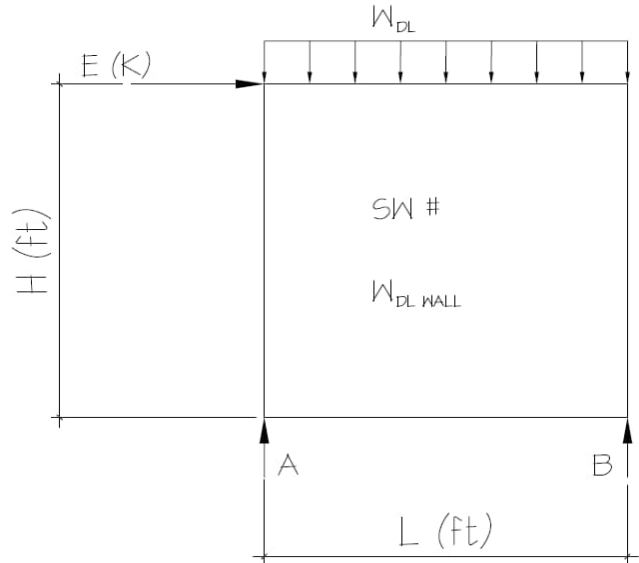
E = 0.90 k

W_{DLWall} = 0.10 kl f

W_{DL} = 0.030 kl f

Ω_0 = 2.5 (ASCE TABLE 12.2.1 FOOTNOTE)

SDS = 1.122



analysis:

E (unfactored) = 1.29

$E_{mh} = \Omega_0 * E = 3.21$ K

$E_v = 0.2 * SDS * DL = 0.344$ K

$E_m = E_{mh} + E_v$

$E_m = E_{mh} + E_v = 3.559$ K

$E_m = E_{mh} - E_v$

$E_m = E_{mh} - E_v = 2.870$ K

E_m (max) = $\sum M_A = 0 = 3.56(9.6) + 0.13(11.8)(5.9) - R_b(11.8)$

$R_b = 0.8DL + 2.9E$

$R_a = 0.8DL - 2.9E$

E_m (min) = $\sum M_A = 0 = 2.87(9.6) + 0.13(11.8)(5.9) - R_b(11.8)$

$R_b = 0.8DL + 2.3E$

$R_a = 0.8DL - 2.3E$

check beams for axial forces shown using load combos per section 12.4.3.1 (asd)

allowable stress permitted to be increased by 1.2

see following beam calcs for load application



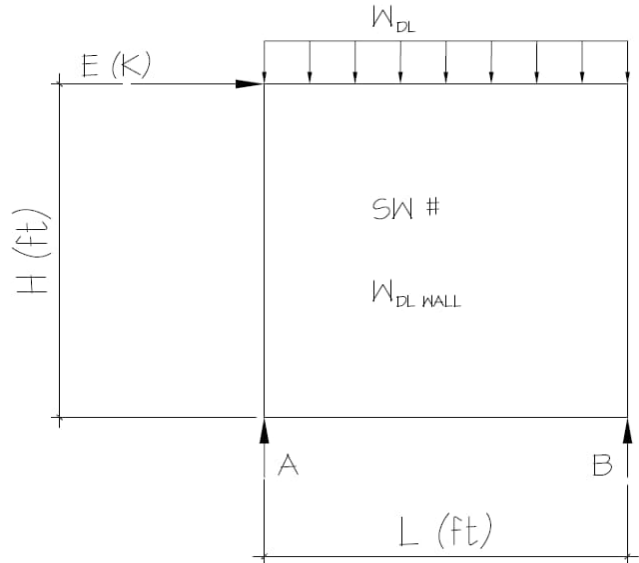
Overstrength Calculations

Wall Description/SW #:

205

Parameters:

- L = 8.0 ft
- H = 10.2 ft
- E = 0.70 k
- W_{DLWall} = 0.10 kl f
- W_{DL} = 0.153 kl f
- Ω_0 = 2.5 (ASCE TABLE 12.2.1 FOOTNOTE)
- SDS = 1.122



analysis:

E (unfactored) = 1.00

$E_{mh} = \Omega_0 * E = 2.50$ K $E_v = 0.2 * SDS * DL = 0.454$ K

$E_m = E_{mh} + E_v = 2.954$ K

$E_m = E_{mh} - E_v = 2.046$ K

$E_m (max) = \sum M_A = 0 = 2.95(10.2) + 0.253(8)(4) - R_b(8)$ $R_b = 1.0DL + 3.8E$

$R_a = 1.0DL - 3.8E$

$E_m (min) = \sum M_A = 0 = 2.05(10.2) + 0.253(8)(4) - R_b(8)$ $R_b = 1.0DL + 2.6E$

$R_a = 1.0DL - 2.6E$

check beams for axial forces shown using load combos per section 12.4.3.1 (asd)

allowable stress permitted to be increased by 1.2

see following beam calcs for load application



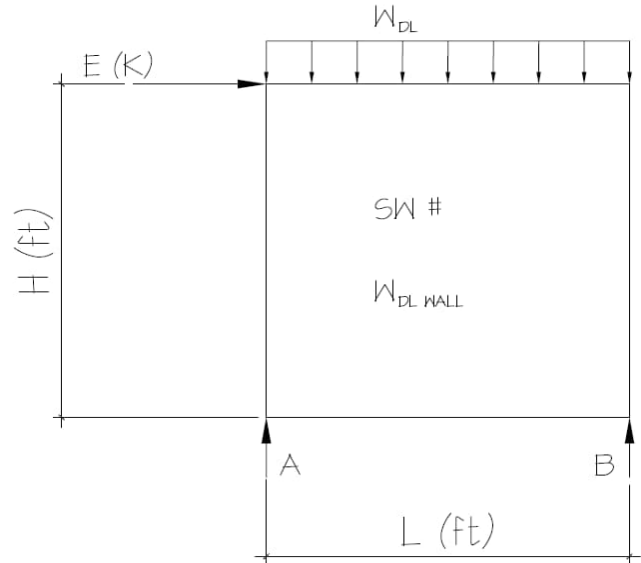
Overstrength Calculations

Wall Description/SW #:

206

Parameters:

L = 6.2 ft
H = 10.5 ft
E = 1.10 k
 W_{DLWall} = 0.10 kl f
 W_{DL} = 0.120 kl f
 Ω_0 = 2.5 (ASCE TABLE 12.2.1 FOOTNOTE)
SDS = 1.122



analysis:

E (unfactored) = 1.57
 $E_{mh} = \Omega_0 * E = 3.93$ K
 $E_v = 0.2 * SDS * DL = 0.306$ K
 $E_m = E_{mh} + E_v = 4.235$ K
 $E_m = E_{mh} - E_v = 3.622$ K

E_m (max) = $\sum M_A = 0 = 4.23(10.5) + 0.22(6.2)(3.1) - R_b(6.2)$ $R_b = 0.7DL + 7.2E$
 $R_a = 0.7DL - 7.2E$

E_m (min) = $\sum M_A = 0 = 3.62(10.5) + 0.22(6.2)(3.1) - R_b(6.2)$ $R_b = 0.7DL + 6.1E$
 $R_a = 0.7DL - 6.1E$

check beams for axial forces shown using load combos per section 12.4.3.1 (asd)

allowable stress permitted to be increased by 1.2

see following beam calcs for load application



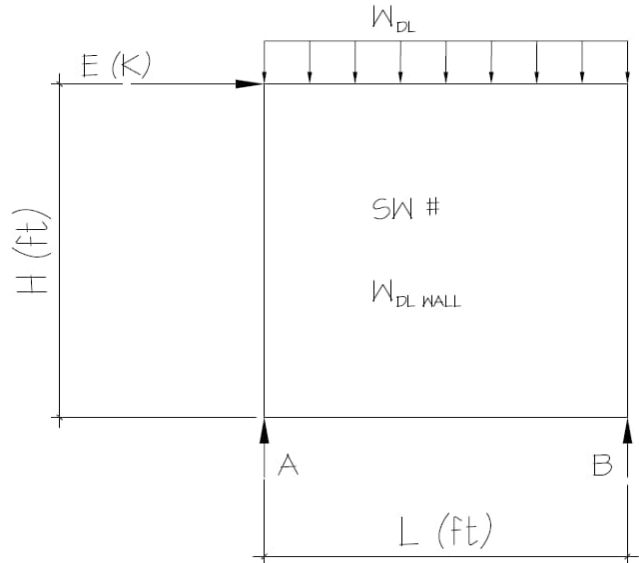
Overstrength Calculations

Wall Description/SW #:

207

Parameters:

- L = 4.3 ft
- H = 9.9 ft
- E = 0.40 k
- W_{DLWall} = 0.10 kl f
- W_{DL} = 0.110 kl f
- Ω_0 = 2.5 (ASCE TABLE 12.2.1 FOOTNOTE)
- SDS = 1.122



analysis:

E (unfactored) = 0.57

$E_{mh} = \Omega_0 * E = 1.43$ K $E_v = 0.2 * SDS * DL = 0.203$ K

$E_m = E_{mh} + E_v = 1.631$ K

$E_m = E_{mh} - E_v = 1.226$ K

E_m (max) = $\sum M_A = 0 = 1.63(9.9) + 0.21(4.3)(2.15) - R_b(4.3)$ $R_b = 0.5DL + 3.8E$
 $R_a = 0.5DL - 3.8E$

E_m (min) = $\sum M_A = 0 = 1.23(9.9) + 0.21(4.3)(2.15) - R_b(4.3)$ $R_b = 0.5DL + 2.8E$
 $R_a = 0.5DL - 2.8E$

check beams for axial forces shown using load combos per section 12.4.3.1 (asd)

allowable stress permitted to be increased by 1.2

see following beam calcs for load application



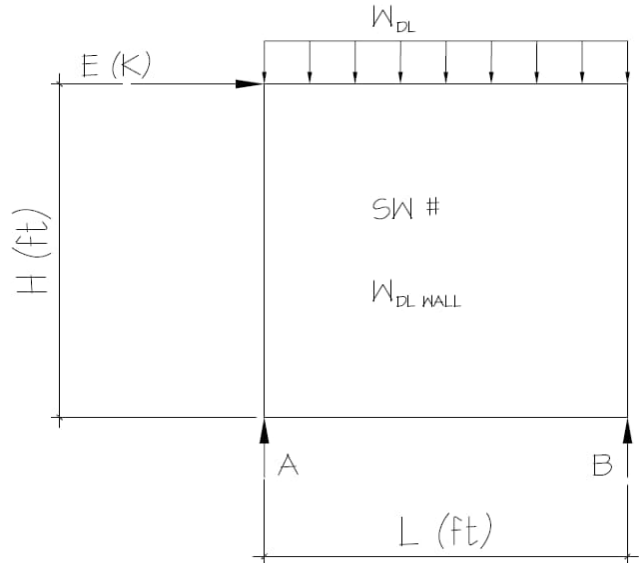
Overstrength Calculations

Wall Description/SW #:

209

Parameters:

- L = 12.4 ft
- H = 9.0 ft
- E = 1.50 k
- W_{DLWall} = 0.10 kl f
- W_{DL} = 0.103 kl f
- Ω_0 = 2.5 (ASCE TABLE 12.2.1 FOOTNOTE)
- SDS = 1.122



analysis:

E (unfactored) = 2.14

$E_{mh} = \Omega_0 * E = 5.36$ K $E_v = 0.2 * SDS * DL = 0.565$ K

$E_m = E_{mh} + E_v = 5.922$ K

$E_m = E_{mh} - E_v = 4.792$ K

$E_m (max) = \sum M_A = 0 = 5.92(9.0) + 0.203(12.4)(6.2) - R_b(12.4)$ $R_b = 1.3DL + 4.3E$

$R_a = 1.3DL - 4.3E$

$E_m (min) = \sum M_A = 0 = 4.79(9.0) + 0.203(12.4)(6.2) - R_b(12.4)$ $R_b = 1.3DL + 3.5E$

$R_a = 1.3DL - 3.5E$

check beams for axial forces shown using load combos per section 12.4.3.1 (asd)

allowable stress permitted to be increased by 1.2

see following beam calcs for load application

Wood Beam

Project File: Calcs.ec6

LIC#: KW-06017913, Build:20.24.05.02

MULHERN & KULP STRUCTURAL ENGINEERING INC

(c) ENERCALC INC 1983-2023

DESCRIPTION: B10 - UPPER FLOOR - FLUSH BM AT REAR GARAGE EXIT (OVERSTRENGTH)

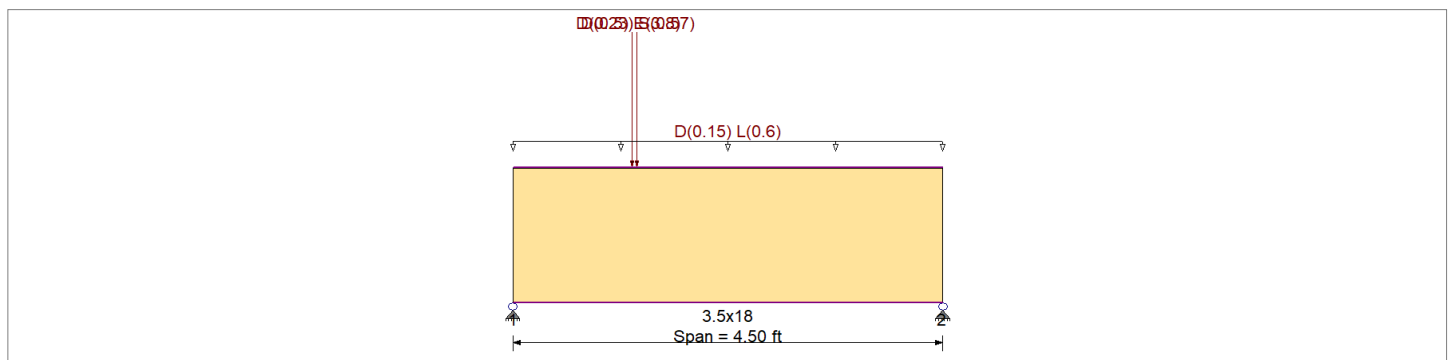
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2021

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2400 psi	E : Modulus of Elasticity	
Load Combination :	IBC 2021	Fb -	1850 psi	Ebend- xx	1800ksi
		Fc - Prll	1650 psi	Eminbend - xx	950ksi
Wood Species :	DF/DF	Fc - Perp	650 psi	Ebend- yy	1600ksi
Wood Grade :	24F-V4	Fv	265 psi	Eminbend - yy	850ksi
		Ft	1100 psi	Density	31.21 pcf
Beam Bracing :	Beam is Fully Braced against lateral-torsional buckling				



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight NOT internally calculated and added

Point Load : D = 0.230, S = 0.570 k @ 1.30 ft

Uniform Load : D = 0.150, L = 0.60 , Tributary Width = 1.0 ft

Point Load : D = 0.50, E = 3.80 k @ 1.250 ft

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio	=	0.067 : 1	Maximum Shear Stress Ratio	=	0.075 : 1
Section used for this span		3.5x18	Section used for this span		3.5x18
fb: Actual	=	258.59psi	fv: Actual	=	31.82 psi
F'b	=	3,840.00psi	F'v	=	424.00 psi
Load Combination	+D+0.750L+0.750S+0.5250E		Load Combination	+D+0.750L+0.750S+0.5250E	
Location of maximum on span	=	1.297ft	Location of maximum on span	=	3.005 ft
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1
Maximum Deflection					
Max Downward Transient Deflection	0.003 in	Ratio = 17375 >=360	Span: 1 : E Only		
Max Upward Transient Deflection	-0.003 in	Ratio = 17375 >=360	Span: 1 : E Only * -1.0		
Max Downward Total Deflection	0.004 in	Ratio = 12279 >=240	Span: 1 : +D+0.750L+0.750S+0.5250E		
Max Upward Total Deflection	-0.002 in	Ratio = 34935 >=240	Span: 1 : +0.60D-0.70E		

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios									Moment Values			Shear Values				
			M	V	CD	CM	C _t	CLx	C _v	C _{fu}	C _i	C _r	M	fb	F'b	V	fv	F'v	
D Only																			
Length = 4.50 ft	1		0.028	0.032	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	0.97	61.5	2,160.0	0.00	0.00	0.0	0.0
+D+L																			
Length = 4.50 ft	1		0.063	0.069	1.00	1.00	1.00	1.00	1.000	1.00	1.00	1.00	2.39	151.7	2,400.0	0.77	18.4	265.0	0.0
+D+S																			
Length = 4.50 ft	1		0.034	0.038	1.15	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.49	94.9	2,760.0	0.48	11.5	304.8	0.0
+D+0.750L																			
Length = 4.50 ft	1		0.043	0.047	1.25	1.00	1.00	1.00	1.000	1.00	1.00	1.00	2.02	128.0	3,000.0	0.66	15.7	331.3	0.0

Wood Beam

Project File: Calcs.ec6

LIC# : KW-06017913, Build:20.24.02.27

MULHERN & KULP STRUCTURAL ENGINEERING INC

(c) ENERCALC INC 1983-2023

DESCRIPTION: B14 - UPPER FLOOR - REAR FLUSH BM @ LIVING

CODE REFERENCES

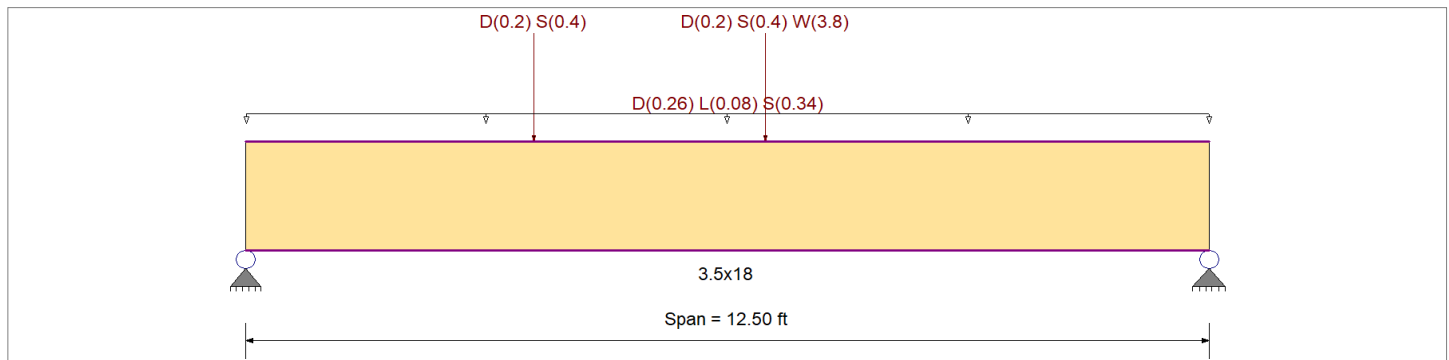
Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2021

Material Properties

Analysis Method : Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity
Load Combination : IBC 2021	Fb -	1,850.0 psi	Ebend- xx
	Fc - Prll	1,650.0 psi	Eminbend - xx
Wood Species : DF/DF	Fc - Perp	650.0 psi	Ebend- yy
Wood Grade : 24F-V4	Fv	265.0 psi	Eminbend - yy
	Ft	1,100.0 psi	Density
			31.210pcf

Beam Bracing : Beam is Fully Braced against lateral-torsional buckling



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : D = 0.260, L = 0.080, S = 0.340, Tributary Width = 1.0 ft

Point Load : D = 0.20, S = 0.40, W = 3.80 k @ 6.750 ft

Point Load : D = 0.20, S = 0.40 k @ 3.750 ft

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio	=	0.341 : 1	Maximum Shear Stress Ratio	=	0.284 : 1
Section used for this span		3.5x18	Section used for this span		3.5x18
fb: Actual	=	942.40psi	fv: Actual	=	86.56 psi
F'b	=	2,760.00psi	F'v	=	304.75 psi
Load Combination		+D+S	Load Combination		+D+S
Location of maximum on span	=	6.387ft	Location of maximum on span	=	0.000 ft
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1
Maximum Deflection					
Max Downward Transient Deflection		0.087 in	Ratio =	1724 >=360	Span: 1 : W Only
Max Upward Transient Deflection		0 in	Ratio =	0 <360	n/a
Max Downward Total Deflection		0.166 in	Ratio =	903 >=240	Span: 1 : +D+0.750L+0.750S+0.450W
Max Upward Total Deflection		0 in	Ratio =	0 <240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios									Moment Values			Shear Values				
			M	V	CD	CM	C _t	CLx	C _v	C _{fu}	C _i	C _r	M	fb	F'b	V	fv	F'v	
D Only	Length = 12.50 ft	1	0.185	0.154	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	6.30	399.8	2,160.0	0.0	0.00	0.0	0.0
+D+L	Length = 12.50 ft	1	0.208	0.173	1.00	1.00	1.00	1.00	1.000	1.00	1.00	1.00	7.86	499.0	2,400.0	0.0	0.00	0.0	0.0
+D+S	Length = 12.50 ft	1	0.341	0.284	1.15	1.00	1.00	1.00	1.000	1.00	1.00	1.00	14.84	942.4	2,760.0	3.64	86.6	304.8	0.0
+D+0.750L	Length = 12.50 ft	1	0.158	0.132	1.25	1.00	1.00	1.00	1.000	1.00	1.00	1.00	7.47	474.2	3,000.0	0.0	0.00	0.0	0.0
+D+0.750L+0.750S	Length = 12.50 ft	1	0.158	0.132	1.25	1.00	1.00	1.00	1.000	1.00	1.00	1.00	7.47	474.2	3,000.0	0.0	0.00	0.0	0.0

Wood Beam

Project File: Calcs.ec6

LIC#: KW-06017913, Build:20.24.02.27

MULHERN & KULP STRUCTURAL ENGINEERING INC

(c) ENERCALC INC 1983-2023

DESCRIPTION: B14 - UPPER FLOOR - REAR FLUSH BM @ LIVING (OVERSTRENGTH)

CODE REFERENCES

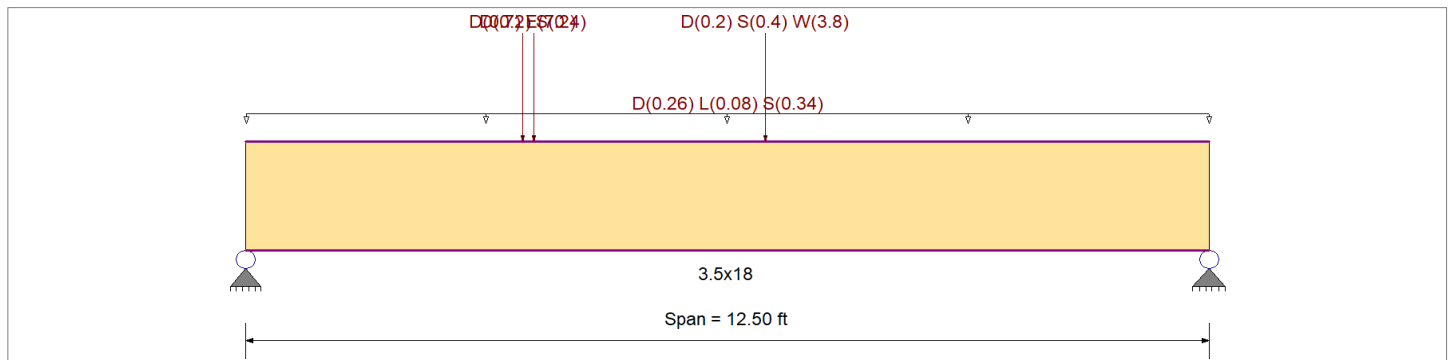
Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2021

Material Properties

Analysis Method : Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity
Load Combination : IBC 2021	Fb -	1,850.0 psi	Ebend- xx
	Fc - Prll	1,650.0 psi	Eminbend - xx
Wood Species : DF/DF	Fc - Perp	650.0 psi	Ebend- yy
Wood Grade : 24F-V4	Fv	265.0 psi	Eminbend - yy
	Ft	1,100.0 psi	Density
			31.210pcf

Beam Bracing : Beam is Fully Braced against lateral-torsional buckling



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading
 Uniform Load : D = 0.260, L = 0.080, S = 0.340, Tributary Width = 1.0 ft
 Point Load : D = 0.20, S = 0.40, W = 3.80 k @ 6.750 ft
 Point Load : D = 0.20, S = 0.40 k @ 3.750 ft
 Point Load : D = 0.70, E = 7.20 k @ 3.60 ft, (OVERSTRENGTH)

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio = 0.383 : 1	Maximum Shear Stress Ratio = 0.370 : 1
Section used for this span = 3.5x18	Section used for this span = 3.5x18
fb: Actual = 1,471.76psi	fv: Actual = 156.89 psi
F'b = 3,840.00psi	F'v = 424.00 psi
Load Combination = +D+0.750L+0.750S+0.5250E	Load Combination = +D+0.750L+0.750S+0.5250E
Location of maximum on span = 4.197ft	Location of maximum on span = 0.000ft
Span # where maximum occurs = Span # 1	Span # where maximum occurs = Span # 1
Maximum Deflection	
Max Downward Transient Deflection = 0.130 in Ratio = 1157 >=360	Span: 1 : E Only
Max Upward Transient Deflection = -0.130 in Ratio = 1157 >=360	Span: 1 : E Only * -1.0
Max Downward Total Deflection = 0.207 in Ratio = 725 >=240	Span: 1 : +D+0.750L+0.750S+0.5250E
Max Upward Total Deflection = -0.049 in Ratio = 3041 >=240	Span: 1 : +0.60D-0.70E

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios										Moment Values			Shear Values				
			M	V	CD	CM	C _t	CLx	C _v	C _{fu}	C _i	C _r	M	fb	F'b	V	fv	F'v		
D Only																				
Length = 12.50 ft	1		0.224	0.204	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	7.61	483.0	2,160.0	0.0	0.00	0.0	0.0	238.5
+D+L																				
Length = 12.50 ft	1		0.242	0.218	1.00	1.00	1.00	1.00	1.000	1.00	1.00	1.00	9.16	581.5	2,400.0	0.0	0.00	0.0	0.0	265.0
+D+S																				
Length = 12.50 ft	1		0.370	0.323	1.15	1.00	1.00	1.00	1.000	1.00	1.00	1.00	16.10	1,022.5	2,760.0	0.0	0.00	0.0	0.0	304.8
+D+0.750L																				
Length = 12.50 ft	1		0.186	0.167	1.25	1.00	1.00	1.00	1.000	1.00	1.00	1.00	8.77	556.8	3,000.0	0.0	0.00	0.0	0.0	331.3

Wood Beam

Project File: Calcs.ec6

LIC# : KW-06017913, Build:20.24.02.27

MULHERN & KULP STRUCTURAL ENGINEERING INC

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DESCRIPTION: B20 - UPPER FLOOR - REAR BM UNDER B.W.A. @ DECK (OVERSTRENGTH)

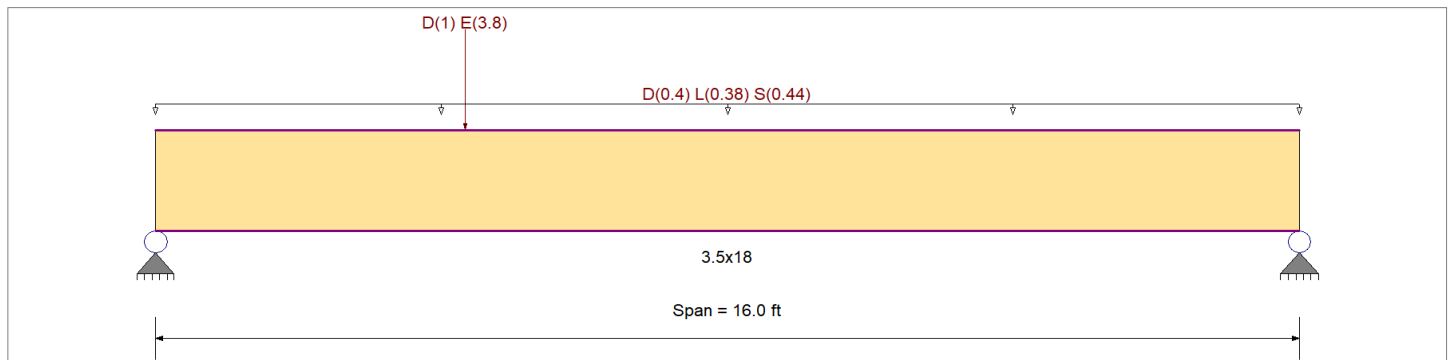
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2021

Material Properties

Analysis Method : Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity	
Load Combination : IBC 2021	Fb -	1,850.0 psi	Ebend- xx	1,800.0ksi
	Fc - Prll	1,650.0 psi	Eminbend - xx	950.0ksi
Wood Species : DF/DF	Fc - Perp	650.0 psi	Ebend- yy	1,600.0ksi
Wood Grade : 24F-V4	Fv	265.0 psi	Eminbend - yy	850.0ksi
	Ft	1,100.0 psi	Density	31.210pcf
Beam Bracing : Beam is Fully Braced against lateral-torsional buckling				



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : D = 0.40, L = 0.380, S = 0.440, Tributary Width = 1.0 ft

Point Load : D = 1.0, E = 3.80 k @ 4.330 ft, (OVERSTRENGTH)

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio	=	0.808 < 1	Maximum Shear Stress Ratio	=	0.583 < 1
Section used for this span		3.5x18	Section used for this span		3.5x18
fb: Actual	=	2,229.66psi	fv: Actual	=	177.55 psi
F'b	=	2,760.00psi	F'v	=	304.75 psi
Load Combination	=	+D+0.750L+0.750S	Load Combination	=	+D+0.750L+0.750S
Location of maximum on span	=	7.708ft	Location of maximum on span	=	0.000 ft
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1
Maximum Deflection					
Max Downward Transient Deflection		0.213 in Ratio = 900 >= 360	Span: 1 : S Only		
Max Upward Transient Deflection		-0.137 in Ratio = 1401 >= 360	Span: 1 : E Only * -1.0		
Max Downward Total Deflection		0.605 in Ratio = 317 >= 240	Span: 1 : +D+0.750L+0.750S+0.5250E		
Max Upward Total Deflection		0 in Ratio = 0 < 240	n/a		

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios										Moment Values			Shear Values				
			M	V	CD	CM	C _t	CLx	C _v	C _{fu}	C _i	C _r	M	fb	F'b	V	fv	F'v		
D Only																				
Length = 16.0 ft	1		0.455	0.343	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	15.49	983.5	2,160.0	0.0	0.00	0.0	0.0	238.5
+D+L																				
Length = 16.0 ft	1		0.730	0.532	1.00	1.00	1.00	1.00	1.000	1.00	1.00	1.00	27.61	1,752.9	2,400.0	0.0	0.00	0.0	0.0	265.0
+D+S																				
Length = 16.0 ft	1		0.679	0.493	1.15	1.00	1.00	1.00	1.000	1.00	1.00	1.00	29.52	1,874.6	2,760.0	0.0	0.00	0.0	0.0	304.8
+D+0.750L																				
Length = 16.0 ft	1		0.520	0.381	1.25	1.00	1.00	1.00	1.000	1.00	1.00	1.00	24.57	1,560.3	3,000.0	0.0	0.00	0.0	0.0	331.3
+D+0.750L+0.750S																				
Length = 16.0 ft	1					1.00	1.00	1.00	1.000	1.00	1.00	1.00			0.0	0.0	0.00	0.0	0.0	0.0

Wood Beam

Project File: Calcs.ec6

LIC# : KW-06017913, Build:20.24.08.01

MULHERN & KULP STRUCTURAL ENGINEERING INC

(c) ENERCALC INC 1983-2023

DESCRIPTION: B20 - UPPER FLOOR - REAR BM UNDER B.W.A. @ DECK

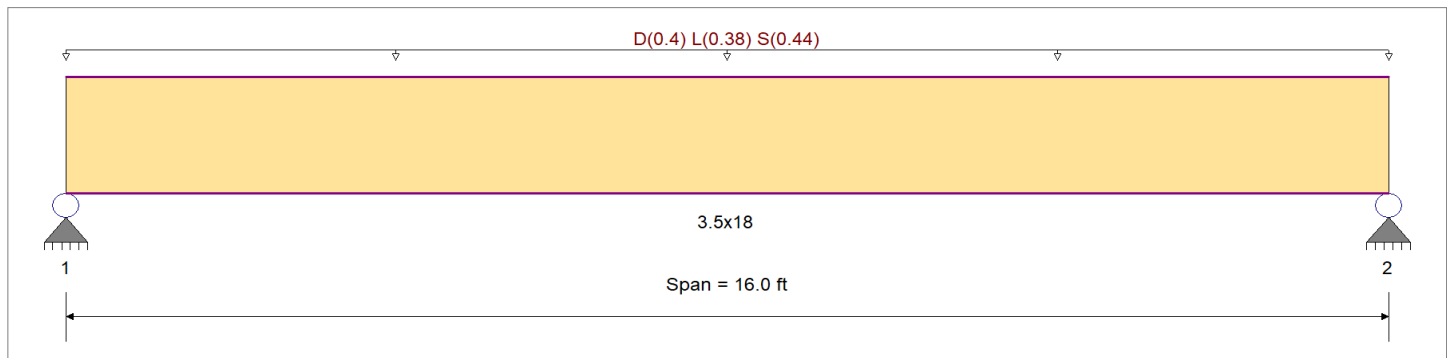
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2021

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity	
Load Combination :	IBC 2021	Fb -	1,850.0 psi	Ebend- xx	1,800.0ksi
		Fc - Prll	1,650.0 psi	Eminbend - xx	950.0ksi
Wood Species :	DF/DF	Fc - Perp	650.0 psi	Ebend- yy	1,600.0ksi
Wood Grade :	24F-V4	Fv	265.0 psi	Eminbend - yy	850.0ksi
		Ft	1,100.0 psi	Density	31.210pcf
Beam Bracing :	Beam is Fully Braced against lateral-torsional buckling				



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : D = 0.40, L = 0.380, S = 0.440 , Tributary Width = 1.0 ft

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio	=	0.757 : 1	Maximum Shear Stress Ratio	=	0.526 : 1
Section used for this span		3.5x18	Section used for this span		3.5x18
fb: Actual	=	2,089.96psi	fv: Actual	=	160.18 psi
F'b	=	2,760.00psi	F'v	=	304.75 psi
Load Combination	=	+D+0.750L+0.750S	Load Combination	=	+D+0.750L+0.750S
Location of maximum on span	=	8.000ft	Location of maximum on span	=	14.540 ft
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1
Maximum Deflection					
Max Downward Transient Deflection		0.213 in Ratio =	900 >=360	Span: 1 : S Only	
Max Upward Transient Deflection		0 in Ratio =	0 <360	n/a	
Max Downward Total Deflection		0.498 in Ratio =	385 >=240	Span: 1 : +D+0.750L+0.750S	
Max Upward Total Deflection		0 in Ratio =	0 <240	n/a	

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios										Moment Values			Shear Values					
			M	V	CD	CM	C _t	CLx	C _v	C _{fu}	C _i	C _r	M	fb	F'b	V	fv	F'v			
D Only																					
Length = 16.0 ft	1	0.389	0.270	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	13.24	840.4	2,160.0	0.0	0.00	0.0	0.0	27.1	64.4	238.5
+D+L																					
Length = 16.0 ft	1	0.672	0.466	1.00	1.00	1.00	1.00	1.000	1.00	1.00	1.00	25.40	1,612.5	2,400.0	0.0	0.00	0.0	0.0	5.19	123.6	265.0
+D+S																					
Length = 16.0 ft	1	0.628	0.436	1.15	1.00	1.00	1.00	1.000	1.00	1.00	1.00	27.32	1,734.4	2,760.0	0.0	0.00	0.0	0.0	5.58	132.9	304.8
+D+0.750L																					
Length = 16.0 ft	1	0.473	0.328	1.25	1.00	1.00	1.00	1.000	1.00	1.00	1.00	22.36	1,419.5	3,000.0	0.0	0.00	0.0	0.0	4.57	108.8	331.3
+D+0.750L+0.750S																					
Length = 16.0 ft	1	0.757	0.526	1.15	1.00	1.00	1.00	1.000	1.00	1.00	1.00	32.92	2,090.0	2,760.0	0.0	0.00	0.0	0.0	6.73	160.2	304.8

Wood Beam

Project File: Calcs.ec6

LIC# : KW-06017913, Build:20.24.08.01

MULHERN & KULP STRUCTURAL ENGINEERING INC

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DESCRIPTION: B21 - UPPER FLOOR - CANT'D BM AT REAR DECK

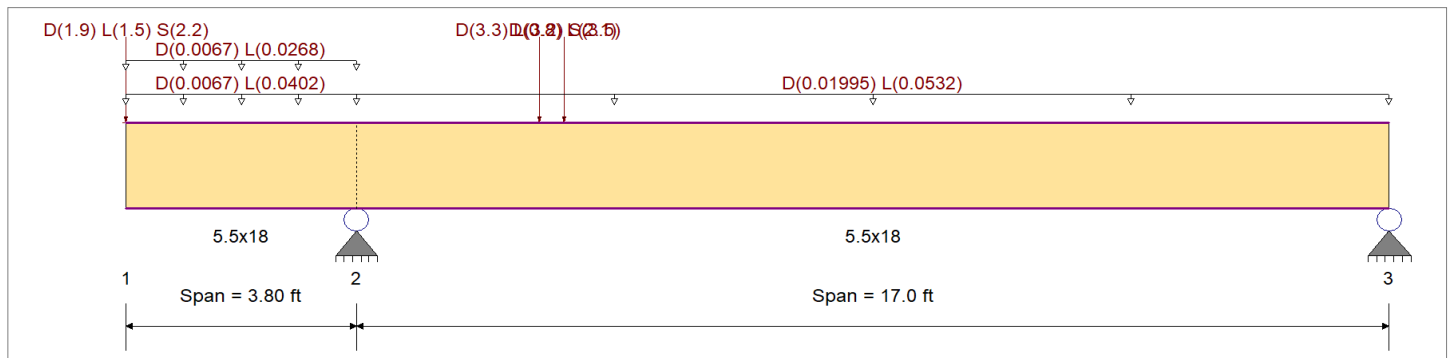
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2021

Material Properties

Analysis Method : Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity	
Load Combination : IBC 2021	Fb -	1,850.0 psi	Ebend- xx	1,800.0ksi
Wood Species : DF/DF	Fc - Prll	1,650.0 psi	Eminbend - xx	950.0ksi
Wood Grade : 24F-V4	Fc - Perp	650.0 psi	Ebend- yy	1,600.0ksi
Beam Bracing : Beam is Fully Braced against lateral-torsional buckling	Fv	265.0 psi	Eminbend - yy	850.0ksi
	Ft	1,100.0 psi	Density	31.210pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Load for Span Number 1

Point Load : D = 1.90, L = 1.50, S = 2.20 k @ 0.0 ft, (B18)

Uniform Load : D = 0.010, L = 0.060 ksf, Tributary Width = 0.670 ft, (DECK)

Uniform Load : D = 0.010, L = 0.040 ksf, Tributary Width = 0.670 ft, (DECK)

Load for Span Number 2

Uniform Load : D = 0.0150, L = 0.040 ksf, Tributary Width = 1.330 ft, (FLOOR)

Point Load : D = 3.30, L = 3.20, S = 3.50 k @ 3.0 ft, (B20)

Point Load : D = 0.80, L = 2.10 k @ 3.410 ft, (B16)

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio	=	0.358 : 1	Maximum Shear Stress Ratio	=	0.523 : 1
Section used for this span		5.5x18	Section used for this span		5.5x18
fb: Actual	=	742.60 psi	fv: Actual	=	138.54 psi
F'b	=	2,071.91 psi	F'v	=	265.00 psi
Load Combination		+D+0.750L+0.750S+H, LL Comb Run (L*)	Load Combination		+D+L+H, LL Comb Run (LL)
Location of maximum on span	=	0.000ft	Location of maximum on span	=	3.800 ft
Span # where maximum occurs	=	Span # 2	Span # where maximum occurs	=	Span # 1
Maximum Deflection					
Max Downward Transient Deflection		0.058 in Ratio = 1562 >=360	Span: 1 : L Only, LL Comb Run (L*)		
Max Upward Transient Deflection		-0.110 in Ratio = 824 >=360	Span: 1 : L Only, LL Comb Run (*L)		
Max Downward Total Deflection		0.174 in Ratio = 1171 >=240	Span: 2 : +D+L+H, LL Comb Run (*L)		
Max Upward Total Deflection		-0.124 in Ratio = 734 >=240	Span: 1 : +D+L+H, LL Comb Run (*L)		

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios										Moment Values			Shear Values				
			M	V	CD	CM	C _t	CLx	C _v	C _{fu}	C _i	C _r	M	fb	F'b	V	fv	F'v		
+D+H																				
	Length = 3.80 ft	1	0.181	0.260	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	7.47	301.9	1,665.0	4.09	62.0	238.5		
	Length = 17.0 ft	2	0.186	0.260	0.90	1.00	1.00	1.00	0.974	1.00	1.00	1.00	7.47	301.9	1,621.5	4.09	62.0	238.5		
+D+L+H, LL Comb Run (*L)						1.00	1.00	1.00	0.974	1.00	1.00	1.00			0.0	0.00	0.0	0.0		

Steel Beam

Project File: Calcs.ec6

LIC#: KW-06017913, Build:20.24.08.01

MULHERN & KULP STRUCTURAL ENGINEERING INC

(c) ENERCALC INC 1983-2023

DESCRIPTION: B21 - UPPER FLOOR - CANT'D BM AT REAR DECK - 2024-09-05 Rev

CODE REFERENCES

Calculations per AISC 360-16, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2021

Material Properties

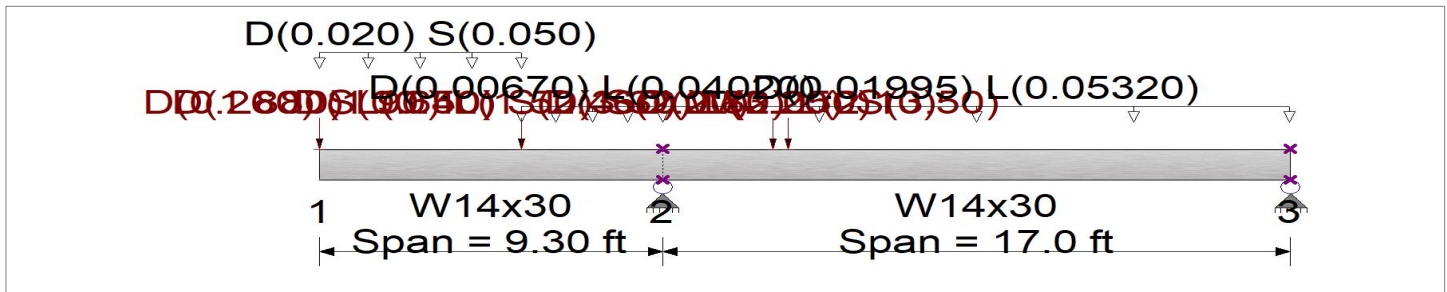
Analysis Method : Allowable Strength Design

Fy : Steel Yield : 50.0 ksi

Beam Bracing : Completely Unbraced

E: Modulus : 29,000.0 ksi

Bending Axis : Major Axis Bending



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Load(s) for Span Number 1

Point Load : D = 1.90, L = 1.50, S = 2.20 k @ 5.50 ft, (B18)

Uniform Load : D = 0.010, L = 0.060 ksf, Extent = 5.50 -->> 9.30 ft, Tributary Width = 0.670 ft, (DECK)

Point Load : D = 0.260, S = 0.640 k @ 0.0 ft, (B13)

Uniform Load : D = 0.010, S = 0.0250 ksf, Extent = 0.0 -->> 5.50 ft, Tributary Width = 2.0 ft, (LOW ROOF)

Point Load : D = 1.880, L = 0.50, S = 2.460, W = 2.050 k @ 5.50 ft, (B14)

Load for Span Number 2

Uniform Load : D = 0.0150, L = 0.040 ksf, Tributary Width = 1.330 ft, (FLOOR)

Point Load : D = 3.30, L = 3.20, S = 3.50 k @ 3.0 ft, (B20)

Point Load : D = 0.80, L = 2.10 k @ 3.410 ft, (B16)

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio =	0.477 : 1	Maximum Shear Stress Ratio =	0.165 : 1
Section used for this span	W14x30	Section used for this span	W14x30
Ma : Applied	47.367 k-ft	Va : Applied	12.305 k
Mn / Omega : Allowable	99.242 k-ft	Vn/Omega : Allowable	74.520 k
Load Combination	+D+0.750L+0.750S+0.450W+H, LL Comb Run (L*)	Load Combination	+D+0.750L+0.750S+0.450W+H, LL Comb Run (LL)
Span # where maximum occurs	Span # 1	Location of maximum on span	9.300 ft
		Span # where maximum occurs	Span # 1
Maximum Deflection			
Max Downward Transient Deflection	0.289 in Ratio = 771 >=360	Span: 2 : S Only	
Max Upward Transient Deflection	-0.154 in Ratio = 1,448 >=360	Span: 2 : L Only, LL Comb Run (*L)	
Max Downward Total Deflection	0.499 in Ratio = 447 >=240.	Span: 2 : +D+0.750L+0.750S+0.450W+H, LL Comb Run (
Max Upward Total Deflection	-0.096 in Ratio = 2119 >=240.	Span: 2 : +D+0.750L+0.750S+0.450W+H, LL Comb Run (

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios		Summary of Moment Values						Summary of Shear Values			
			M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx	Vnx/Omega
+D+H														
Dsgn. L =	9.30 ft	1	0.190	0.066		-18.85	18.85	165.73	99.24	1.00	1.00	4.89	111.78	74.52
Dsgn. L =	17.00 ft	2	0.160	0.066	0.03	-18.85	18.85	197.08	118.01	3.00	1.00	4.89	111.78	74.52
+D+L+H, LL Comb Run (*L)														
Dsgn. L =	9.30 ft	1	0.190	0.130		-18.85	18.85	165.73	99.24	1.00	1.00	9.66	111.78	74.52
Dsgn. L =	17.00 ft	2	0.179	0.130	10.81	-18.85	18.85	176.23	105.53	1.79	1.00	9.66	111.78	74.52
+D+L+H, LL Comb Run (L*)														
Dsgn. L =	9.30 ft	1	0.269	0.089		-26.74	26.74	165.73	99.24	1.00	1.00	6.61	111.78	74.52
Dsgn. L =	17.00 ft	2	0.227	0.072		-26.74	26.74	197.08	118.01	2.73	1.00	5.35	111.78	74.52
+D+L+H, LL Comb Run (LL)														
Dsgn. L =	9.30 ft	1	0.269	0.136		-26.74	26.74	165.73	99.24	1.00	1.00	10.12	111.78	74.52
Dsgn. L =	17.00 ft	2	0.227	0.136	5.17	-26.74	26.74	197.08	118.01	2.99	1.00	10.12	111.78	74.52
+D+Lr+H, LL Comb Run (*L)														
Dsgn. L =	9.30 ft	1	0.190	0.066		-18.85	18.85	165.73	99.24	1.00	1.00	4.89	111.78	74.52
Dsgn. L =	17.00 ft	2	0.160	0.066	0.03	-18.85	18.85	197.08	118.01	3.00	1.00	4.89	111.78	74.52

Steel Beam

Project File: Calcs.ec6

LIC#: KW-06017913, Build:20.24.08.01

MULHERN & KULP STRUCTURAL ENGINEERING INC

(c) ENERCALC INC 1983-2023

DESCRIPTION: B21 - UPPER FLOOR - CANT'D BM AT REAR DECK - 2024-09-05 Rev (OVERSTRENGTH)

CODE REFERENCES

Calculations per AISC 360-16, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2021

Material Properties

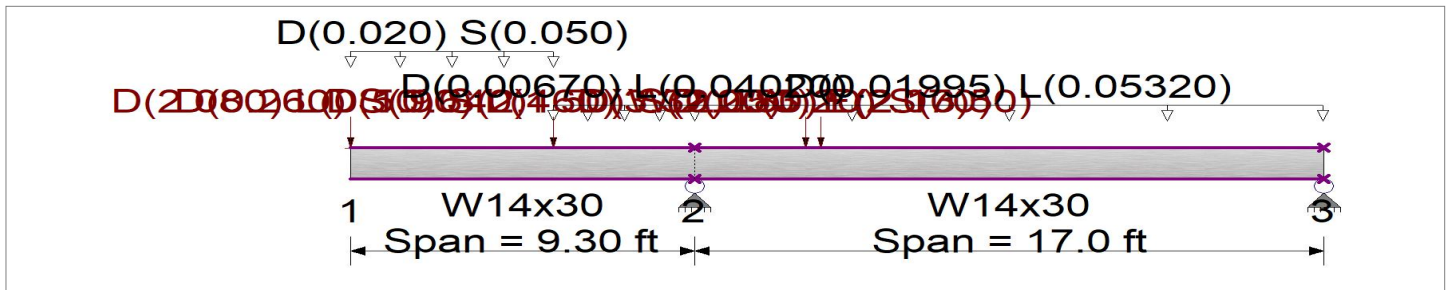
Analysis Method : Allowable Strength Design

Fy : Steel Yield : 50.0 ksi

Beam Bracing : Beam is Fully Braced against lateral-torsional buckling

E: Modulus : 29,000.0 ksi

Bending Axis : Major Axis Bending



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Load(s) for Span Number 1

Point Load : D = 1.90, L = 1.50, S = 2.20 k @ 5.50 ft, (B18)

Uniform Load : D = 0.010, L = 0.060 ksf, Extent = 5.50 -->> 9.30 ft, Tributary Width = 0.670 ft, (DECK)

Point Load : D = 0.260, S = 0.640 k @ 0.0 ft, (B13)

Uniform Load : D = 0.010, S = 0.0250 ksf, Extent = 0.0 -->> 5.50 ft, Tributary Width = 2.0 ft, (LOW ROOF)

Point Load : D = 2.080, L = 0.50, S = 2.460, W = 2.050, E = 2.070 k @ 5.50 ft, (B14)

Load for Span Number 2

Uniform Load : D = 0.0150, L = 0.040 ksf, Tributary Width = 1.330 ft, (FLOOR)

Point Load : D = 3.30, L = 3.20, S = 3.50 k @ 3.0 ft, (B20)

Point Load : D = 0.80, L = 2.10 k @ 3.410 ft, (B16)

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio =	0.413 : 1	Maximum Shear Stress Ratio =	0.166 : 1
Section used for this span	W14x30	Section used for this span	W14x30
Ma : Applied	48.751 k-ft	Va : Applied	12.386 k
Mn / Omega : Allowable	118.014 k-ft	Vn/Omega : Allowable	74.520 k
Load Combination	0.750L+0.750S+0.5250E+H, LL Comb Run (L*)	Load Combination	0.750L+0.750S+0.5250E+H, LL Comb Run (LL)
Span # where maximum occurs	Span # 1	Location of maximum on span	9.300 ft
		Span # where maximum occurs	Span # 1
Maximum Deflection			
Max Downward Transient Deflection	0.289 in Ratio = 771 >=360	Span: 2 : S Only	
Max Upward Transient Deflection	-0.154 in Ratio = 1,448 >=360	Span: 2 : L Only, LL Comb Run (*L)	
Max Downward Total Deflection	0.518 in Ratio = 431 >=180	Span: 2 : +D+0.750L+0.750S+0.5250E+H, LL Comb Run	
Max Upward Total Deflection	-0.102 in Ratio = 2008 >=180	Span: 2 : +D+0.750L+0.750S+0.5250E+H, LL Comb Run	

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios		Summary of Moment Values						Summary of Shear Values			
			M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx	Vnx/Omega
+D+H														
Dsgn. L =	9.30 ft	1	0.166	0.066		-19.61	19.61	197.08	118.01	1.00	1.00	4.94	111.78	74.52
Dsgn. L =	17.00 ft	2	0.166	0.066	0.00	-19.61	19.61	197.08	118.01	1.00	1.00	4.94	111.78	74.52
+D+L+H, LL Comb Run (*L)														
Dsgn. L =	9.30 ft	1	0.166	0.130		-19.61	19.61	197.08	118.01	1.00	1.00	9.70	111.78	74.52
Dsgn. L =	17.00 ft	2	0.166	0.130	10.21	-19.61	19.61	197.08	118.01	1.00	1.00	9.70	111.78	74.52
+D+L+H, LL Comb Run (L*)														
Dsgn. L =	9.30 ft	1	0.233	0.091		-27.50	27.50	197.08	118.01	1.00	1.00	6.81	111.78	74.52
Dsgn. L =	17.00 ft	2	0.233	0.072		-27.50	27.50	197.08	118.01	1.00	1.00	5.40	111.78	74.52
+D+L+H, LL Comb Run (LL)														
Dsgn. L =	9.30 ft	1	0.233	0.136		-27.50	27.50	197.08	118.01	1.00	1.00	10.17	111.78	74.52
Dsgn. L =	17.00 ft	2	0.233	0.136	4.73	-27.50	27.50	197.08	118.01	1.00	1.00	10.17	111.78	74.52
+D+Lr+H, LL Comb Run (*L)														
Dsgn. L =	9.30 ft	1	0.166	0.066		-19.61	19.61	197.08	118.01	1.00	1.00	4.94	111.78	74.52
Dsgn. L =	17.00 ft	2	0.166	0.066	0.00	-19.61	19.61	197.08	118.01	1.00	1.00	4.94	111.78	74.52

Wood Beam

Project File: Calcs.ec6

LIC#: KW-06017913, Build:20.24.02.27

MULHERN & KULP STRUCTURAL ENGINEERING INC

(c) ENERCALC INC 1983-2023

DESCRIPTION: B22 - UPPER FLOOR - BM ABOVE KITCHEN

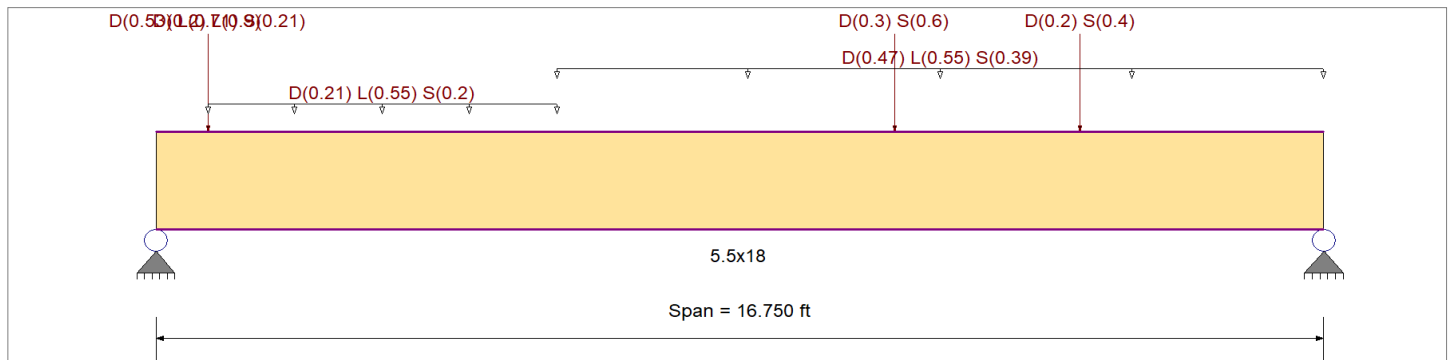
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2021

Material Properties

Analysis Method : Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity	
Load Combination : IBC 2021	Fb -	1,850.0 psi	Ebend- xx	1,800.0ksi
	Fc - Prll	1,650.0 psi	Eminbend - xx	950.0ksi
Wood Species : DF/DF	Fc - Perp	650.0 psi	Ebend- yy	1,600.0ksi
Wood Grade : 24F-V4	Fv	265.0 psi	Eminbend - yy	850.0ksi
	Ft	1,100.0 psi	Density	31.210pcf
Beam Bracing : Beam is Fully Braced against lateral-torsional buckling				



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Point Load : D = 0.530, L = 0.710, S = 0.210 k @ 0.750 ft, (B21)

Point Load : D = 0.20, L = 0.90, S = 0.50 k @ 0.750 ft, (BEAM)

Uniform Load : D = 0.210, L = 0.550, S = 0.20 k/ft, Extent = 0.750 --> 5.750 ft, Tributary Width = 1.0 ft, (FLOOR)

Point Load : D = 0.30, S = 0.60 k @ 10.60 ft, (P.A.)

Point Load : D = 0.20, S = 0.40 k @ 13.250 ft, (P.A.)

Uniform Load : D = 0.470, L = 0.550, S = 0.390 k/ft, Extent = 5.750 --> 16.750 ft, Tributary Width = 1.0 ft, (WALL ABOVE)

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio	=	0.643	1	Maximum Shear Stress Ratio	=	0.439	1
Section used for this span		5.5x18		Section used for this span		5.5x18	
fb: Actual	=	1,730.30psi		fv: Actual	=	133.87 psi	
F'b	=	2,691.87psi		F'v	=	304.75 psi	
Load Combination	=	+D+0.750L+0.750S		Load Combination	=	+D+0.750L+0.750S	
Location of maximum on span	=	8.925ft		Location of maximum on span	=	15.283 ft	
Span # where maximum occurs	=	Span # 1		Span # where maximum occurs	=	Span # 1	
Maximum Deflection							
Max Downward Transient Deflection		0.210 in	Ratio =	955	>=	360	Span: 1 : L Only
Max Upward Transient Deflection		0 in	Ratio =	0	<	360	n/a
Max Downward Total Deflection		0.449 in	Ratio =	447	>=	240	Span: 1 : +D+0.750L+0.750S
Max Upward Total Deflection		0 in	Ratio =	0	<	240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios									Moment Values			Shear Values				
			M	V	CD	CM	C _t	CLx	C _v	C _{fu}	C _i	C _r	M	fb	F'b	V	fv	F'v	
D Only	Length = 16.750 ft	1	0.321	0.223	0.90	1.00	1.00	1.00	0.975	1.00	1.00	1.00	16.75	676.7	2,106.7	0.0	0.00	0.0	0.0
+D+L	Length = 16.750 ft	1	0.629	0.422	1.00	1.00	1.00	1.00	0.975	1.00	1.00	1.00	36.47	1,473.4	2,340.8	0.0	0.00	0.0	0.0
+D+S	Length = 16.750 ft	1	0.479	0.335	1.15	1.00	1.00	1.00	0.975	1.00	1.00	1.00	31.90	1,288.7	2,691.9	6.75	102.2	304.8	0.0

Wood Beam

Project File: Calcs.ec6

LIC# : KW-06017913, Build:20.24.02.27

MULHERN & KULP STRUCTURAL ENGINEERING INC

(c) ENERCALC INC 1983-2023

DESCRIPTION: B26 - UPPER FLOOR - EDGE BEAM @ B.W.A. @ FRONT PORCH (OVERSTRENGTH)

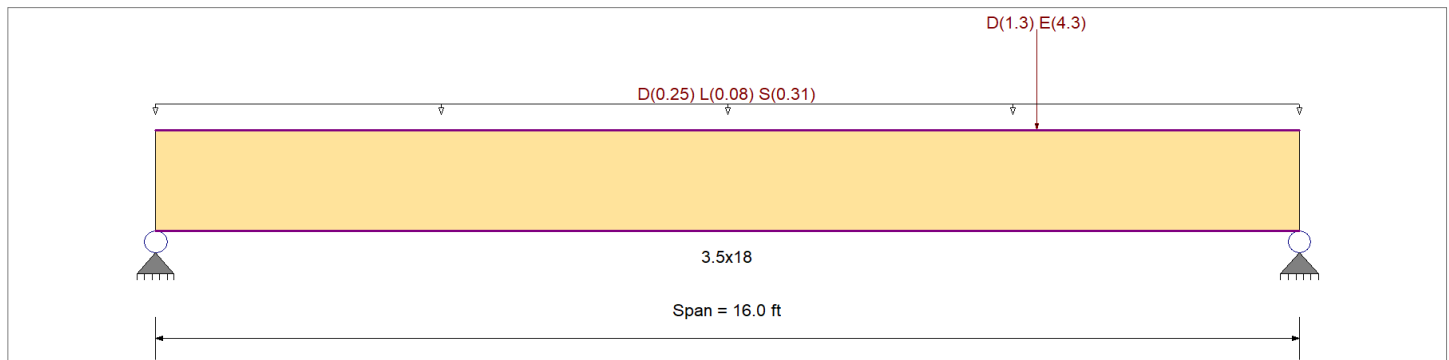
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2021

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity	
Load Combination :	IBC 2021	Fb -	1,850.0 psi	Ebend- xx	1,800.0ksi
		Fc - Prll	1,650.0 psi	Eminbend - xx	950.0ksi
Wood Species :	DF/DF	Fc - Perp	650.0 psi	Ebend- yy	1,600.0ksi
Wood Grade :	24F-V4	Fv	265.0 psi	Eminbend - yy	850.0ksi
		Ft	1,100.0 psi	Density	31.210pcf
Beam Bracing :	Beam is Fully Braced against lateral-torsional buckling				



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : D = 0.250, L = 0.080, S = 0.310, Tributary Width = 1.0 ft

Point Load : D = 1.30, E = 4.30 k @ 12.330 ft, (OVERSTRENGTH)

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio	=	0.479	1	Maximum Shear Stress Ratio	=	0.371	1
Section used for this span		3.5x18		Section used for this span		3.5x18	
fb: Actual	=	1,321.90psi		fv: Actual	=	113.18 psi	
F'b	=	2,760.00psi		F'v	=	304.75 psi	
Load Combination		+D+S		Load Combination		+D+S	
Location of maximum on span	=	8.526ft		Location of maximum on span	=	14.540 ft	
Span # where maximum occurs	=	Span # 1		Span # where maximum occurs	=	Span # 1	
Maximum Deflection							
Max Downward Transient Deflection		0.150 in	Ratio =	1278	>=	360	Span: 1 : S Only
Max Upward Transient Deflection		-0.136 in	Ratio =	1416	>=	360	Span: 1 : E Only * -1.0
Max Downward Total Deflection		0.380 in	Ratio =	505	>=	240	Span: 1 : +D+0.750L+0.750S+0.5250E
Max Upward Total Deflection		-0.003 in	Ratio =	60941	>=	240	Span: 1 : +0.60D-0.70E

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios										Moment Values			Shear Values				
			M	V	CD	CM	C _t	CLx	C _v	C _{fu}	C _i	C _r	M	fb	F'b	V	fv	F'v		
D Only																				
Length = 16.0 ft	1		0.323	0.272	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	10.99	697.8	2,160.0	0.0	0.00	0.0	0.0	238.5
+D+L																				
Length = 16.0 ft	1		0.357	0.292	1.00	1.00	1.00	1.00	1.000	1.00	1.00	1.00	13.51	857.9	2,400.0	0.0	0.00	0.0	0.0	265.0
+D+S																				
Length = 16.0 ft	1		0.479	0.371	1.15	1.00	1.00	1.00	1.000	1.00	1.00	1.00	20.82	1,321.9	2,760.0	0.0	0.00	0.0	0.0	304.8
+D+0.750L																				
Length = 16.0 ft	1		0.273	0.224	1.25	1.00	1.00	1.00	1.000	1.00	1.00	1.00	12.88	817.8	3,000.0	0.0	0.00	0.0	0.0	331.3
+D+0.750L+0.750S																				
Length = 16.0 ft	1					1.00	1.00	1.00	1.000	1.00	1.00	1.00			0.0	0.00	0.0	0.0	0.0	0.0

Wood Beam

Project File: Calcs.ec6

LIC# : KW-06017913, Build:20.24.02.27

MULHERN & KULP STRUCTURAL ENGINEERING INC

(c) ENERCALC INC 1983-2023

DESCRIPTION: B34 - UPPER FLOOR - BM ABOVE KITCHEN

CODE REFERENCES

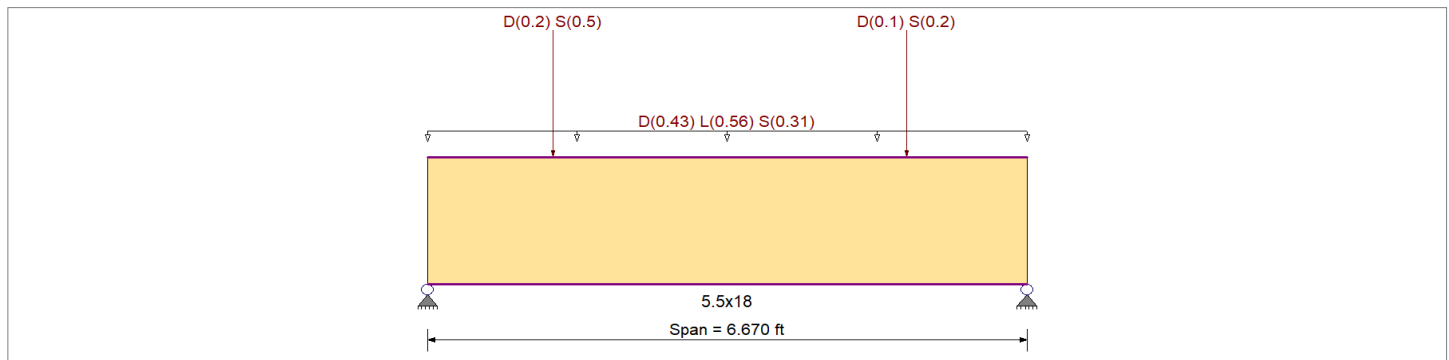
Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2021

Material Properties

Analysis Method : Allowable Stress Design	Fb +	2,400.0 psi	<i>E : Modulus of Elasticity</i>
Load Combination : IBC 2021	Fb -	1,850.0 psi	Ebend- xx
	Fc - Prll	1,650.0 psi	Eminbend - xx
Wood Species : DF/DF	Fc - Perp	650.0 psi	Ebend- yy
Wood Grade : 24F-V4	Fv	265.0 psi	Eminbend - yy
	Ft	1,100.0 psi	Density
			31.210pcf

Beam Bracing : Beam is Fully Braced against lateral-torsional buckling



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : D = 0.430, L = 0.560, S = 0.310, Tributary Width = 1.0 ft

Point Load : D = 0.20, S = 0.50 k @ 1.40 ft

Point Load : D = 0.10, S = 0.20 k @ 5.330 ft

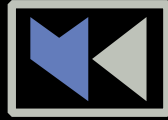
DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio	=	0.098	1	Maximum Shear Stress Ratio	=	0.108	1
Section used for this span		5.5x18		Section used for this span		5.5x18	
fb: Actual	=	271.17 psi		fv: Actual	=	28.68 psi	
F'b	=	2,760.00 psi		F'v	=	265.00 psi	
Load Combination	=	+D+0.750L+0.750S		Load Combination	=	+D+L	
Location of maximum on span	=	3.262ft		Location of maximum on span	=	5.185 ft	
Span # where maximum occurs	=	Span # 1		Span # where maximum occurs	=	Span # 1	
Maximum Deflection							
Max Downward Transient Deflection		0.005 in	Ratio =	15352	>=	360	Span: 1 : L Only
Max Upward Transient Deflection		0 in	Ratio =	0	<	360	n/a
Max Downward Total Deflection		0.011 in	Ratio =	7046	>=	240	Span: 1 : +D+0.750L+0.750S
Max Upward Total Deflection		0 in	Ratio =	0	<	240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios									Moment Values			Shear Values					
			M	V	CD	CM	C _t	CLx	C _v	C _{fu}	C _i	C _r	M	fb	F'b	V	fv	F'v		
D Only	Length = 6.670 ft	1	0.051	0.054	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	2.72	109.8	2,160.0	0.00	0.00	0.0	0.0	238.5
+D+L	Length = 6.670 ft	1	0.098	0.108	1.00	1.00	1.00	1.00	1.000	1.00	1.00	1.00	5.83	235.6	2,400.0	1.89	28.7	265.0	0.0	0.0
+D+S	Length = 6.670 ft	1	0.072	0.074	1.15	1.00	1.00	1.00	1.000	1.00	1.00	1.00	4.93	199.2	2,760.0	1.50	22.7	304.8	0.0	0.0
+D+0.750L	Length = 6.670 ft	1	0.068	0.075	1.25	1.00	1.00	1.00	1.000	1.00	1.00	1.00	5.05	204.2	3,000.0	1.63	24.8	331.3	0.0	0.0
+D+0.750L+0.750S	Length = 6.670 ft	1	0.068	0.075	1.25	1.00	1.00	1.00	1.000	1.00	1.00	1.00	5.05	204.2	3,000.0	1.63	24.8	331.3	0.0	0.0



MULHERN+KULP
RESIDENTIAL STRUCTURAL ENGINEERING

Shear Wall Calculations

LNL Builds

27xx 62nd Ave

Mercer Island, Washington

Parameters:

Single Family Home

Design Wind Speed: 100 MPH

wind Exposure Category: C

Seismic Design Category: D

Code & Design Standard: 2018 IBC Ch. 1609, ASCE 7-16 Ch. 26-30

MULHERN & KULP STRUCTURAL ENGINEERING, INC.

NJM

Matthew Mills, Staff Engineer

SEISMIC CALCULATION - ASCE 7-16

Seismic Design Category:

User Inputs:

Site Class	D
Spectral Response Accel. 0.2 sec, S_s	1.402
Spectral Response Accel. 1.0 sec, S₁	0.488
Occupancy Category	II

Variables:

Site coefficient, F _a	1.20
Site coefficient, F _v	1.81

Calculated Values:

Maximum spectral response acceleration, S_{ms}	1.682
Maximum spectral response acceleration, S_{m1}	0.884
Design spectral response acceleration, S_{ds}	1.122
Design spectral response acceleration, S_{d1}	0.590
Seismic Design Category (short term)	D
Seismic Design Category (1.0 second term)	D

Building period Determination:

User Inputs:

Building period coefficient, C_t	0.020
Long-Period Trans Period, T_L (sec)	6
Ht. abv base to highest level, h _n	23

Calculated Values:

Approximate Fundamental Period, T _a	0.211
T ₀	0.105
T _s	0.526
Spectral Response Acc., S _a (g)	1.122

Site Class Assumption

Yes	Per ASCE 7-16 Section 11.4.3 the Site Class may be assumed to be D
-----	--------------------------------------------------------------------

Equivalent lateral force procedure

Dead Load Calculation:

Level	Story Ht. (ft.)	Area (ft ²)	Dead Load (psf)	DL of ext wall trib. to level (kips)	Total Level DL
1	11.5	1553	15	15.7	39 k
2	11.7	1836	10	7.9	26 k
3	0.0	0	0	0.0	0 k
4	0.0	0	0	0.0	0 k
5	0.0	0	0	0.0	0 k
6	0.0	0	0	0.0	0 k
7	0.0	0	0	0.0	0 k
8	0.0	0	0	0.0	0 k
9	0.0	0	0	0.0	0 k
10	0.0	0	0	0.0	0 k
11	0.0	0	0	0.0	0 k
12	0.0	0	0	0.0	0 k
13	0.0	0	0	0.0	0 k
14	0.0	0	0	0.0	0 k
15	0.0	0	0	0.0	0 k
16	0.0	0	0	0.0	0 k
17	0.0	0	0	0.0	0 k
18	0.0	0	0	0.0	0 k
19	0.0	0	0	0.0	0 k
20	0.0	0	0	0.0	0 k

Total Dead Load Of Structure = 65 Kips

Seismic Response Coefficient:

	Transverse	Longitudinal
Response modification factor, R	6.5	6.5
Occupancy Importance Factor, I_E	1.00	1.00
Seismic Response Coefficient, C_s	0.173	0.173

Base Shears:

Ultimate Loads

Transverse	Longitudinal
11 k	11 k

x 0.7 =

Allowable Loads

Transverse	Longitudinal
7.9 k	7.9 k

Story Shear Calculation:

Distribution exponent, 1.00

Ultimate Loads

Level	Vert. Dist. Factor, C_{vk}	Transverse		Longitudinal	
		Story Shear, F _x	Σ Story Shear	Story Shear, F _x	Σ Story Shear
1	0.424	4.8 k	4.8 k	4.8 k	4.8 k
2	0.576	6.5 k	6.5 k	6.5 k	6.5 k
3	0.000	0.0 k	0.0 k	0.0 k	0.0 k
4	0.000	0.0 k	0.0 k	0.0 k	0.0 k
5	0.00	0.0 k	0.0 k	0.0 k	0.0 k
6	0.00	0.0 k	0.0 k	0.0 k	0.0 k
7	0.00	0.0 k	0.0 k	0.0 k	0.0 k
8	0.00	0.0 k	0.0 k	0.0 k	0.0 k
9	0.00	0.0 k	0.0 k	0.0 k	0.0 k
10	0.00	0.0 k	0.0 k	0.0 k	0.0 k
11	0.00	0.0 k	0.0 k	0.0 k	0.0 k
12	0.00	0.0 k	0.0 k	0.0 k	0.0 k
13	0.00	0.0 k	0.0 k	0.0 k	0.0 k
14	0.00	0.0 k	0.0 k	0.0 k	0.0 k
15	0.00	0.0 k	0.0 k	0.0 k	0.0 k
16	0.00	0.0 k	0.0 k	0.0 k	0.0 k
17	0.00	0.0 k	0.0 k	0.0 k	0.0 k
18	0.00	0.0 k	0.0 k	0.0 k	0.0 k
19	0.00	0.0 k	0.0 k	0.0 k	0.0 k
20	0.00	0.0 k	0.0 k	0.0 k	0.0 k

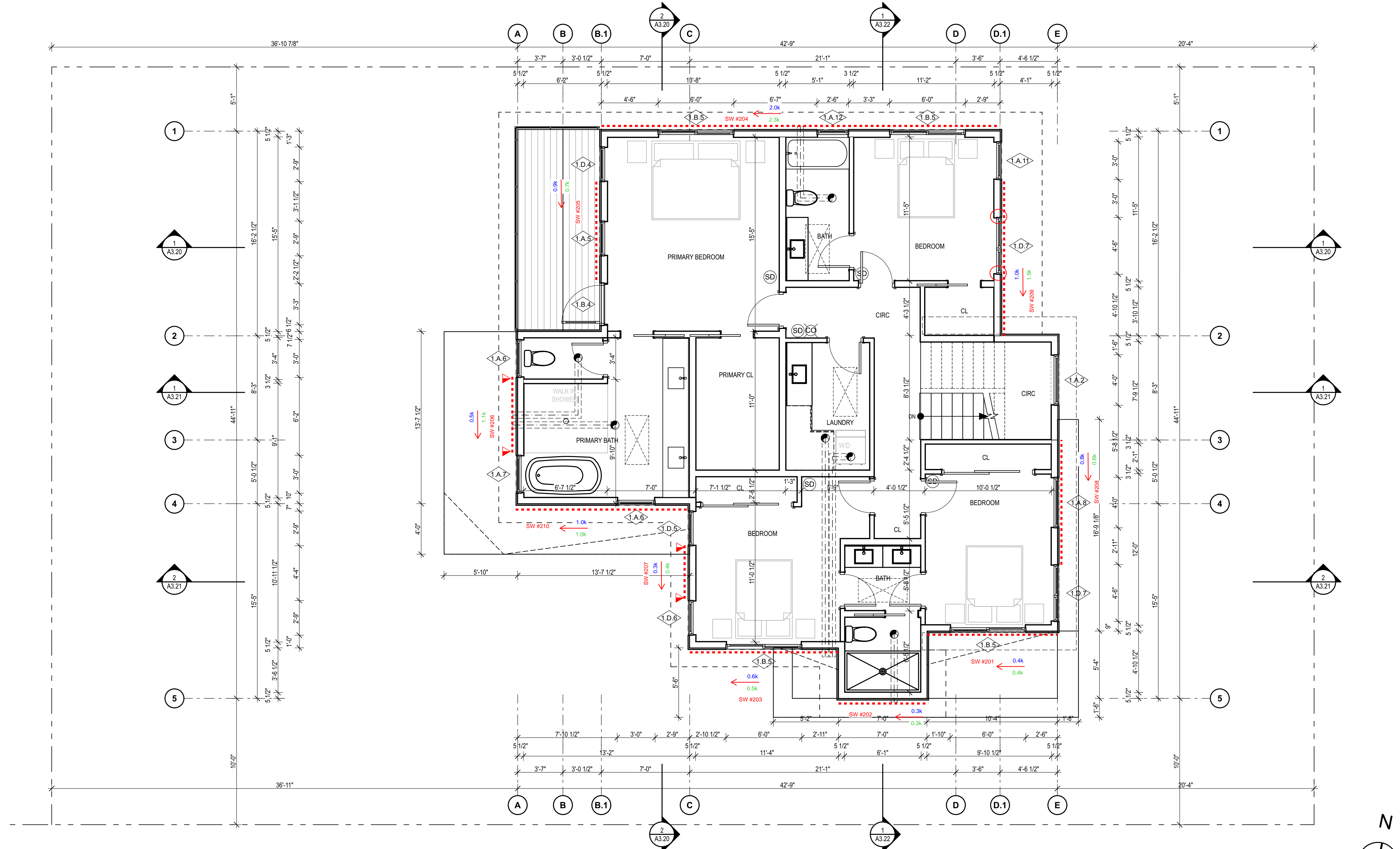
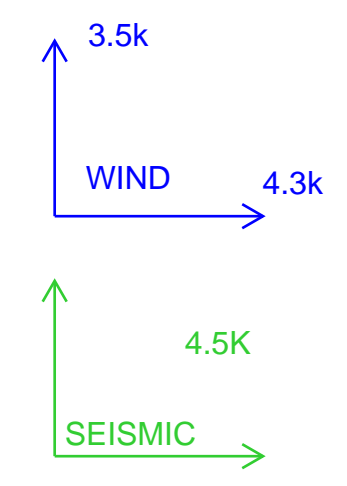
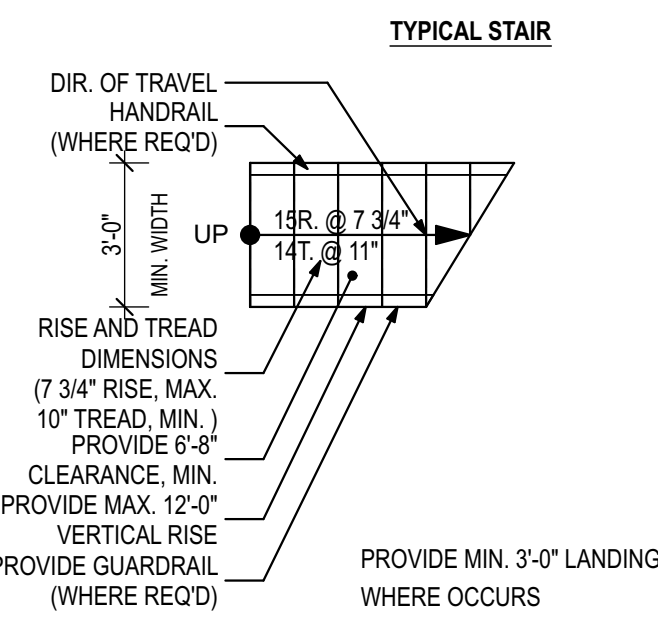
x 0.7 =

Allowable Loads

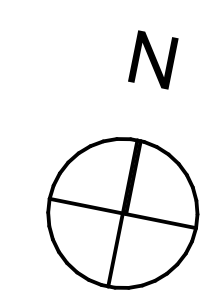
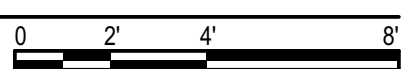
Transverse		Longitudinal	
Story Shear, F _x	Σ Story Shear	Story Shear, F _x	Σ Story Shear
3.3 k	7.9 k	3.3 k	7.9 k
4.5 k	4.5 k	4.5 k	4.5 k
0.0 k	0.0 k	0.0 k	0.0 k
0.0 k	0.0 k	0.0 k	0.0 k
0.0 k	0.0 k	0.0 k	0.0 k
0.0 k	0.0 k	0.0 k	0.0 k
0.0 k	0.0 k	0.0 k	0.0 k
0.0 k	0.0 k	0.0 k	0.0 k
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0.0 k	0.0 k	0.0 k	0.0 k
0.0 k	0.0 k	0.0 k	0.0 k
0.0 k	0.0 k	0.0 k	0.0 k
0.0 k	0.0 k	0.0 k	0.0 k
0.0 k	0.0 k	0.0 k	0.0 k
0.0 k	0.0 k	0.0 k	0.0 k
0.0 k	0.0 k	0.0 k	0.0 k
0.0 k	0.0 k	0.0 k	0.0 k
0.0 k	0.0 k	0.0 k	0.0 k
0.0 k	0.0 k	0.0 k	0.0 k
0.0 k	0.0 k	0.0 k	0.0 k

PLAN LEGEND

DOOR DESIGNATION 1.1	DOOR WIDTH		1-HOUR FIRE-RESISTANCE RATED CONSTRUCTION 2 X 4 FRAMING	(SD)	SRC R314: SMOKE ALARMS SHALL BE INSTALLED IN THE FOLLOWING LOCATIONS: 1. IN EACH SLEEPING ROOM 2. OUTSIDE EACH SEPARATE SLEEPING AREA IN THE IMMEDIATE VICINITY OF THE BEDROOMS. 3. ON EACH ADDITIONAL STORY OF THE DWELLING INCLUDING BASEMENTS BUT NOT INCLUDING CRAWL SPACES. 4. PER SFC 907.2.10 SMOKE ALARMS SHALL BE INSTALLED 20" MIN FROM KITCHEN APPLIANCES OR 10" MIN WITH AN ALARM-SILENCING SWITCH, 3" MIN FROM BATHROOM DOORS. 5. SMOKE ALARMS REQUIRED TO BE INSTALLED, HARDWIRED AND INTERCONNECTED, TYP.
WINDOW DESIGNATION 1.1	WINDOW WIDTH 3'-0" WINDOW HEIGHT 5'-0"		1-HOUR FIRE-RESISTANCE RATED CONSTRUCTION 2 X 6 FRAMING	(SD _{sw})	SMOKE ALARM WITH SWITCH, PER ITEM 4 ABOVE
	DETAIL NUMBER SHEET NUMBER		CAST-IN-PLACE CONCRETE WALL	(SD _{fan})	FAN LOCATION (SRC TABLE M 1505.4.4(1)) 1. AT BATHROOMS AND LAUNDRY, PROVIDE 50 CFM FAN W/ TIMER AT 0.25 W.G. OR GREATER 2. AT KITCHENS, PROVIDE 100 CFM FAN AT 0.25 W.G. OR GREATER 3. VENT ALL EXHAUST FANS TO THE OUTSIDE 4. EXHAUST DUCTS ARE TO BE CONST. OF SMOOTH BORE NONCOMBUSTIBLE MATERIAL AND ARE TO BE INSUL. AS REQUIRED PER WSEC.
	SECTION MARKER		PROVIDE (1) LAYER 5/8" EXTERIOR GWB AT OVERHANG	(SD _{cc})	SRC R315 AND 2018 SFC 915: AN APPROVED CARBON MONOXIDE ALARM SHALL BE INSTALLED OUTSIDE OF EACH SEPARATE SLEEPING AREA IN THE IMMEDIATE VICINITY OF THE BEDROOMS IN DWELLING UNITS AND ON EACH LEVEL OF THE DWELLING. SINGLE STATION CARBON MONOXIDE ALARMS SHALL BE LISTED AS COMPLYING WITH UL 2075. SRC R315.5. CARBON MONOXIDE ALARMS REQUIRED TO BE INSTALLED, HARDWIRED AND INTERCONNECTED, TYP.
	FLOOR STEP DOWN		PROVIDE CMU WALL	(WD)	WASHING/ DRYER MACHINE (COMBO)
	SOFFIT STEP DOWN		PROVIDE MIN. 3'-0" LANDING WHERE OCCURS	(HWH)	ON-DEMAND HOT WATER HEATER
				(HD)	HEAT DETECTOR/HEAT ALARM PER SRC R314.2.1



1 SECOND FLOOR PLAN
SCALE: 1/4" = 1'-0"

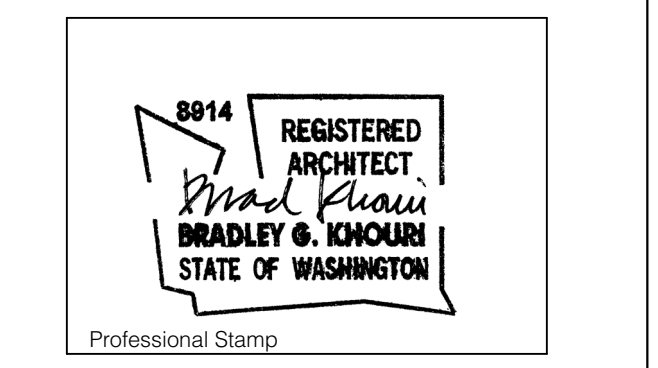


Architect of Record
b9 architects
610 2nd Avenue
Seattle, WA 98104
206.297.1284
www.b9architects.com

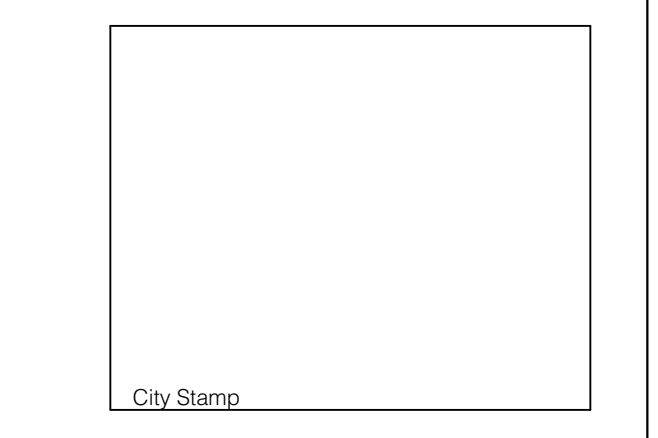
Project:
2740 61st Ave SE

Location:
2740 61ST AVE SE
MERCER ISLAND, WA 98040

SDCI Number:
#SDCI CN#



Issue ID	Issue Name	Issue Date



Second Floor Plan

A2.02



Shearwall Design Summary

M+K Project #: 300-24003

Engineer: MPM

Shearwall 201: 2nd - South Bedroom Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
 Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
 fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL plf Overturning Moment k-ft Hold Down Design Load lbs
 DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required

Shearwall 202: 2nd - South Bathroom Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
 Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
 fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL plf Overturning Moment k-ft Hold Down Design Load lbs
 DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required



Shearwall 203: 2nd - South Bedroom Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required

Shearwall 204: 2nd - North Bedrooms Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required



Shearwall 205: 2nd - Deck Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required

Shearwall 206: 2nd - Primary Bath Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

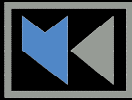
P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

SIMPSON CS16 STRAP TIE (14" END LENGTH)



Shearwall 207: 2nd - South Bedroom Rear Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

SIMPSON CS16 STRAP TIE (14" END LENGTH)

Shearwall 208: 2nd - South Bedroom Front Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required



Shearwall Design Summary

M+K Project #: 300-24003
Engineer: MPM

Shearwall 209: 2nd - North Bedroom Front Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required

Shearwall 101: 1st - Garage South Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required



Shearwall 102: 1st - Living Room South Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL plf Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required

Shearwall 103: 1st - North Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL plf Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required



Shearwall 104: 1st - Dining Rear Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P3 - 1-side 7/16" OSB
fastened w/ 8d nails at 3"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

SIMPSON STHD14RJ HOLDOWN

Shearwall 105: 1st - Dining Rear Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P3 - 1-side 7/16" OSB
fastened w/ 8d nails at 3"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

SIMPSON STHD14RJ HOLDOWN



Shearwall Design Summary

M+K Project #: 300-24003
Engineer: MPM

Shearwall 106: 1st - Garage Rear Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

SIMPSON STHD14RJ HOLDOWN

Shearwall 107: 1st - Bath Front Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

SIMPSON STHD14RJ HOLDOWN



Shearwall 210: 2nd - Primary Bath Side Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL plf Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required

Shearwall 108: 1st - Outdoor Shed Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL plf Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required



Shearwall 109: 1st - Outdoor Shed Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL plf Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

SIMPSON STHD14RJ HOLDDOWN

Shearwall 110: 1st - Int. Garage Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

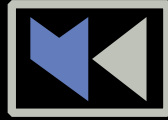
P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL plf Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required



MULHERN+KULP
RESIDENTIAL STRUCTURAL ENGINEERING

Shear Wall Calculations

LNL Builds

27xx 62nd Ave

Mercer Island, Washington

Parameters:

Single Family Home

Design Wind Speed: 100 MPH

wind Exposure Category: C

Seismic Design Category: D

Code & Design Standard: 2018 IBC Ch. 1609, ASCE 7-16 Ch. 26-30

MULHERN & KULP STRUCTURAL ENGINEERING, INC.

NJM

Matthew Mills, Staff Engineer

Wind Design Summary per ASCE 7-16

Parameters:

Wind Speed	100
Exposure Category	C
Risk Category	II
Wind Directionality Factor, K_d	0.85
Topographic Factor, K_{zt}	1.00
Gust Factor, G	0.85
Ground El. Above Sea Level [ft]	0
Design Type	ASD

 0.60

Roof Geometry:

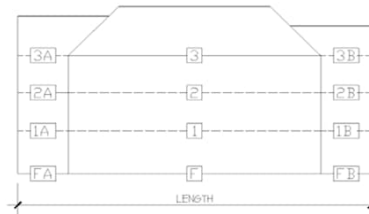
Trans. Roof Pitch	0.3	:12
Long. Roof Pitch	0.3	:12
Mean Roof Height, H	23.67	ft

Building Geometry:

length	45	ft
Width	41	ft
Number of stories	2	

Transverse Direction (Perpendicular to Main Ridge Line)

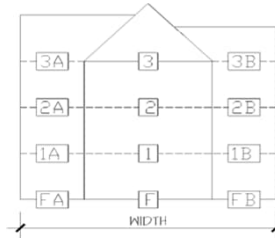
Diaphragm Level	Floor-to-Floor Height	Roof Surface	Tributary Design Areas:			sq ft
			Section			
		A O B				
2	11.67 ft	Roof Surface	0	0	0	sq ft
		Wall surface	0	263	0	sq ft
1	11.5 ft	Roof Surface	0	0	0	sq ft
		Wall surface	0	512	0	sq ft
FND		Roof Surface	0	0	0	sq ft
		Wall surface	0	0	0	sq ft



	Tributary Design Loads: (0.6W)			kips		
	Section					
		A O B				
Story Shear	0.00	3.54	0.00	kips		
Total Shear	0.00	3.54	0.00	kips		
		3.54				
Story Shear	0.00	6.51	0.00	kips		
Total Shear	0.00	10.05	0.00	kips		
		10.05				
Story Shear	0.00	0.00	0.00	kips		
Total Shear	0.00	10.05	0.00	kips		
		10.05				

Longitudinal Direction (Parallel to Main Ridge Line)

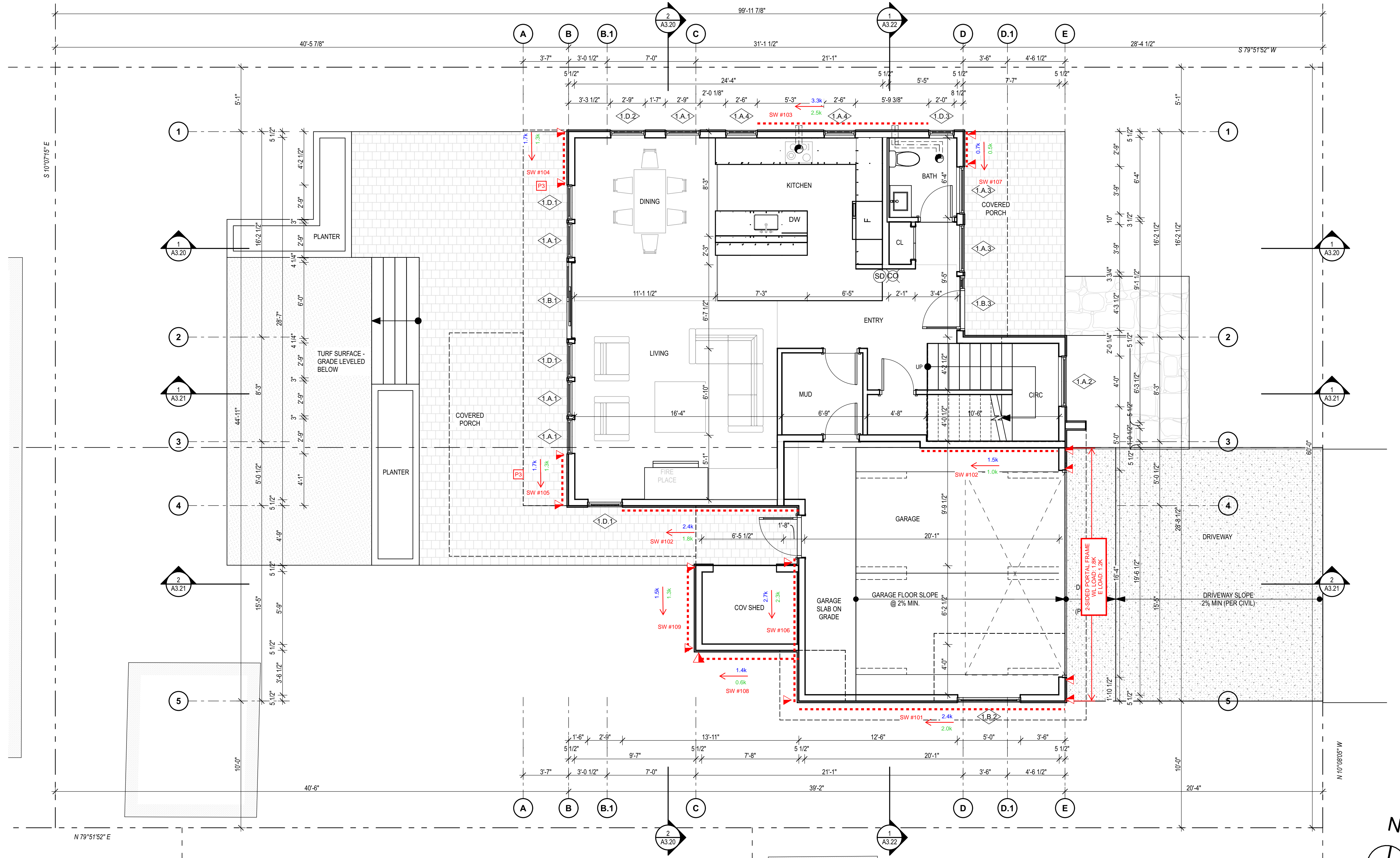
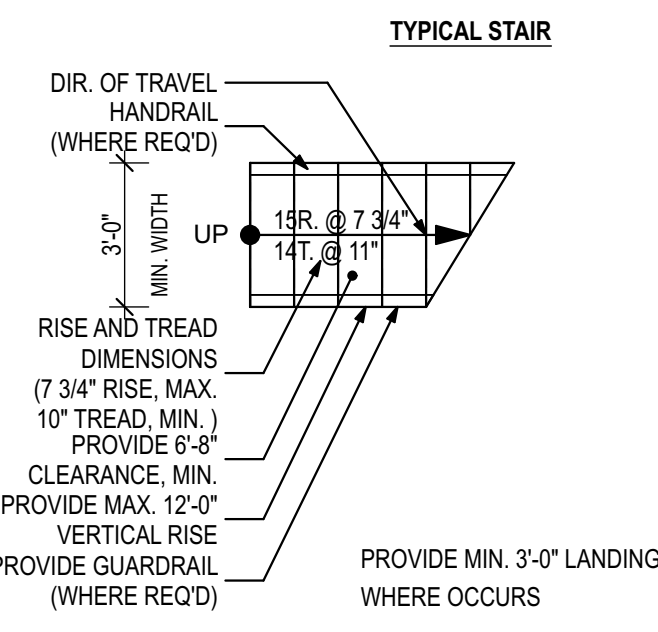
Diaphragm Level	Floor-to-Floor Height	Roof Surface	Tributary Design Areas:			sq ft
			Section			
		A O B				
2	11.67 ft	Roof Surface	0	0	0	sq ft
		Wall surface	0	324	0	sq ft
1	11.5 ft	Roof Surface	0	0	0	sq ft
		Wall surface	0	530	0	sq ft
FND		Roof Surface	0	0	0	sq ft
		Wall surface	0	0	0	sq ft



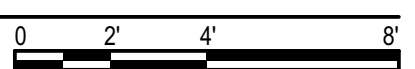
	Tributary Design Loads: (0.6W)			kips		
	Section					
		A O B				
Story Shear	0.00	4.29	0.00	kips		
Total Shear	0.00	4.29	0.00	kips		
		4.29				
Story Shear	0.00	6.64	0.00	kips		
Total Shear	0.00	10.93	0.00	kips		
		10.93				
Story Shear	0.00	0.00	0.00	kips		
Total Shear	0.00	10.93	0.00	kips		
		10.93				

PLAN LEGEND

DOOR DESIGNATION 1.1	DOOR WIDTH		1-HOUR FIRE-RESISTANCE RATED CONSTRUCTION 2 X 4 FRAMING	(SD)	SRC R314: SMOKE ALARMS SHALL BE INSTALLED IN THE FOLLOWING LOCATIONS: 1. IN EACH SLEEPING ROOM 2. OUTSIDE EACH SEPARATE SLEEPING AREA IN THE IMMEDIATE VICINITY OF THE BEDROOMS 3. ON EACH ADDITIONAL STORY OF THE DWELLING INCLUDING BASEMENTS BUT NOT INCLUDING CRAWL SPACES 4. PER SFC 907.2.10 SMOKE ALARMS SHALL BE INSTALLED 20" MIN FROM KITCHEN APPLIANCES OR 10" MIN WITH AN ALARM-SILENCING SWITCH, 3" MIN FROM BATHROOM DOORS 5. SMOKE ALARMS REQUIRED TO BE INSTALLED, HARDWIRED AND INTERCONNECTED, TYP.
WINDOW DESIGNATION 1.1	WINDOW WIDTH 3'-0" WINDOW HEIGHT 5'-0"		1-HOUR FIRE-RESISTANCE RATED CONSTRUCTION 2 X 6 FRAMING	(SD _{sw})	SMOKE ALARM WITH SWITCH, PER ITEM 4 ABOVE
	DETAIL NUMBER SHEET NUMBER		CAST-IN-PLACE CONCRETE WALL	(FAN)	FAN LOCATION (SRC TABLE M 1505.4.4(1)) 1. AT BATHROOMS AND LAUNDRY, PROVIDE 50 CFM FAN W/ TIMER AT 0.25 W.G. OR GREATER 2. AT KITCHENS, PROVIDE 100 CFM FAN AT 0.25 W.G. OR GREATER 3. VENT ALL EXHAUST FANS TO THE OUTSIDE 4. EXHAUST DUCTS ARE TO BE CONST. OF SMOOTH BORE NONCOMBUSTIBLE MATERIAL AND ARE TO BE INSUL. AS REQUIRED PER WSEC.
	SECTION MARKER		PROVIDE (1) LAYER 5/8" EXTERIOR GWB AT OVERHANG	(CO)	CO CARBON MONOXIDE ALARM PER SRC R315.2.1
	FLOOR STEP DOWN		PROVIDE CMU WALL	(WD)	WASHING/ DRYER MACHINE (COMBO)
	SOFFIT STEP DOWN		PROVIDE ON-DEMAND HOT WATER HEATER	(HD)	HEAT DETECTOR/HEAT ALARM PER SRC R314.2.1



1 FIRST FLOOR PLAN
SCALE: 1/4" = 1'-0"

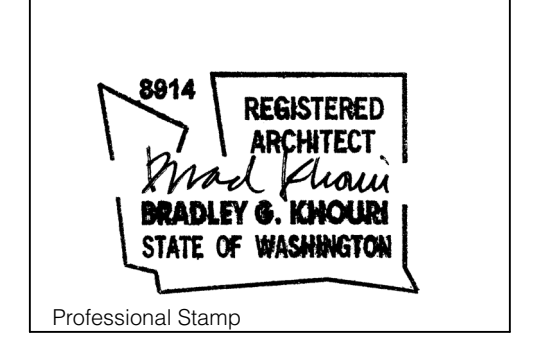


Architect of Record
b9 architects
610 2nd Avenue
Seattle, WA 98104
206.297.1284
www.b9architects.com

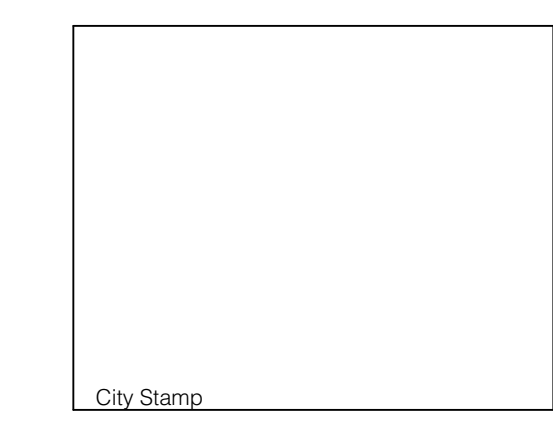
Project:
2740 61st Ave SE

Location:
2740 61ST AVE SE
MERCER ISLAND, WA 98040

SDCI Number:
#SDCI CN#



Issue ID	Issue Name	Issue Date

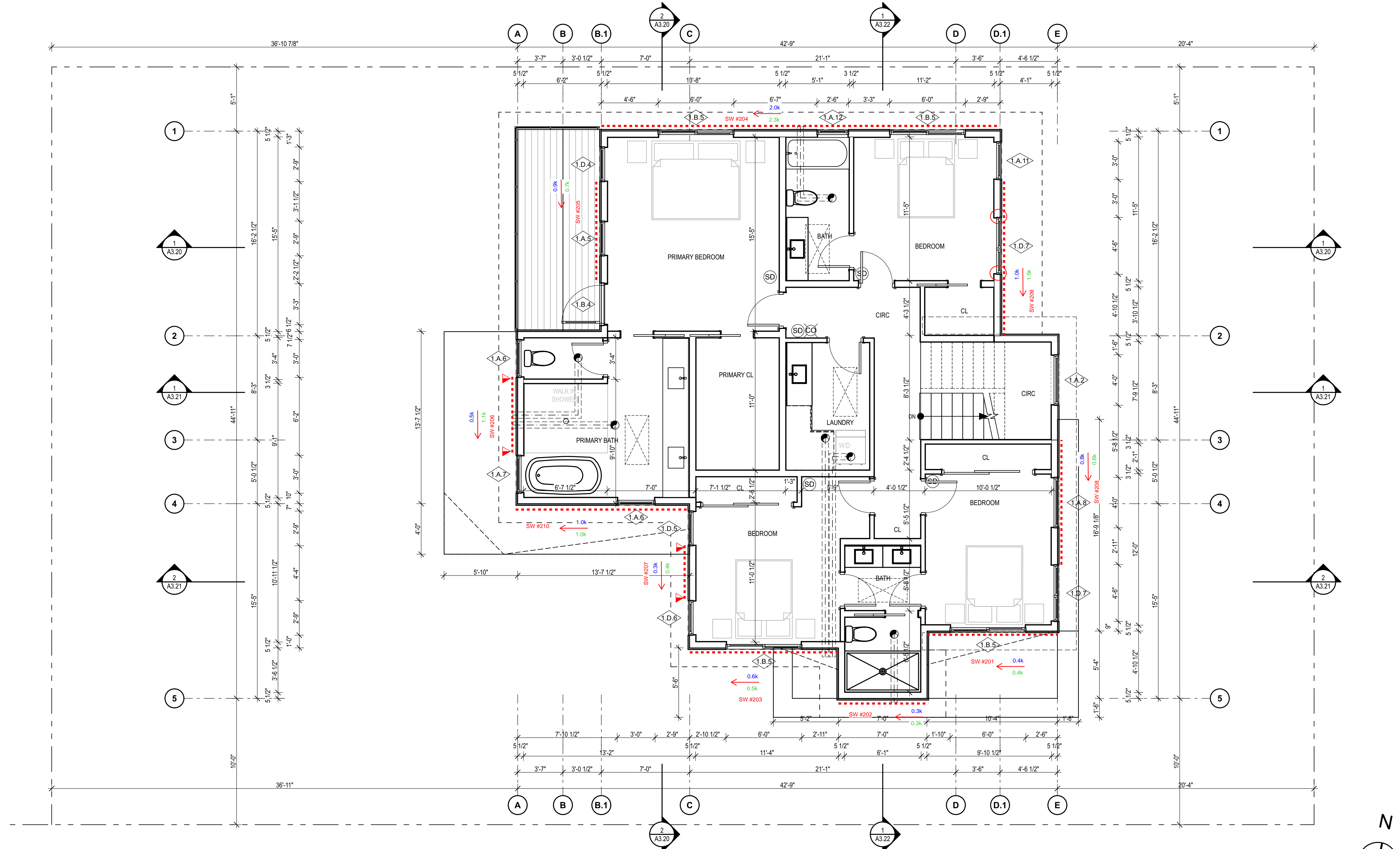
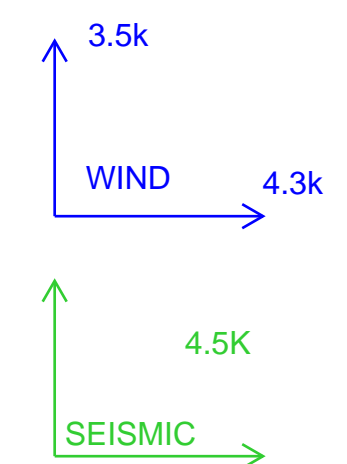
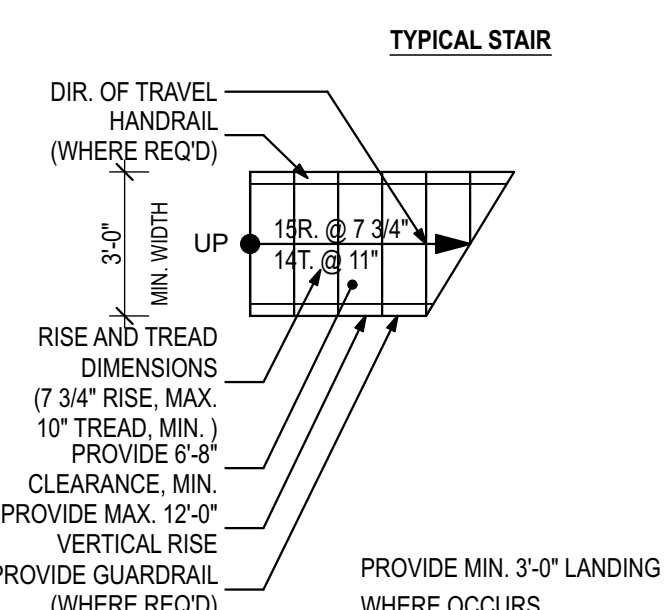


First Floor Plan

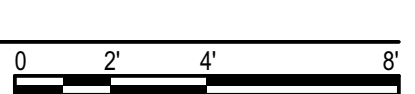
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PLAN LEGEND

DOOR DESIGNATION 1.1	DOOR WIDTH		1-HOUR FIRE-RESISTANCE RATED CONSTRUCTION 2 X 4 FRAMING	(SD)	SRC R314: SMOKE ALARMS SHALL BE INSTALLED IN THE FOLLOWING LOCATIONS: 1. IN EACH SLEEPING ROOM 2. OUTSIDE EACH SEPARATE SLEEPING AREA IN THE IMMEDIATE VICINITY OF THE BEDROOMS. 3. ON EACH ADDITIONAL STORY OF THE DWELLING INCLUDING BASEMENTS BUT NOT INCLUDING CRAWL SPACES. 4. PER SFC 907.2.10 SMOKE ALARMS SHALL BE INSTALLED 20" MIN FROM KITCHEN APPLIANCES OR 10" MIN WITH AN ALARM-SILENCING SWITCH, 3" MIN FROM BATHROOM DOORS. 5. SMOKE ALARMS REQUIRED TO BE INSTALLED, HARDWIRED AND INTERCONNECTED, TYP.
WINDOW DESIGNATION 1.1	WINDOW WIDTH 3'-0" WINDOW HEIGHT 5'-0"		1-HOUR FIRE-RESISTANCE RATED CONSTRUCTION 2 X 6 FRAMING	(SD _{sw})	SMOKE ALARM WITH SWITCH, PER ITEM 4 ABOVE
	DETAIL NUMBER SHEET NUMBER		CAST-IN-PLACE CONCRETE WALL	(SD _{fan})	FAN LOCATION (SRC TABLE M 1505.4.4(1)) 1. AT BATHROOMS AND LAUNDRY, PROVIDE 50 CFM FAN W/ TIMER AT 0.25 W.G. OR GREATER 2. AT KITCHENS, PROVIDE 100 CFM FAN AT 0.25 W.G. OR GREATER 3. VENT ALL EXHAUST FANS TO THE OUTSIDE 4. EXHAUST DUCTS ARE TO BE CONST. OF SMOOTH BORE NONCOMBUSTIBLE MATERIAL AND ARE TO BE INSUL. AS REQUIRED PER WSEC.
	SECTION MARKER		PROVIDE (1) LAYER 5/8" EXTERIOR GWB AT OVERHANG	(SD _{cc})	SRC R315 AND 2018 SFC 915: AN APPROVED CARBON MONOXIDE ALARM SHALL BE INSTALLED OUTSIDE OF EACH SEPARATE SLEEPING AREA IN THE IMMEDIATE VICINITY OF THE BEDROOMS IN DWELLING UNITS AND ON EACH LEVEL OF THE DWELLING. SINGLE STATION CARBON MONOXIDE ALARMS SHALL BE LISTED AS COMPLYING WITH UL 2075. SRC R315.5. CARBON MONOXIDE ALARMS REQUIRED TO BE INSTALLED, HARDWIRED AND INTERCONNECTED, TYP.
	FLOOR STEP DOWN		PROVIDE CMU WALL	(WD)	WASHING/ DRYER MACHINE (COMBO)
	SOFFIT STEP DOWN		PROVIDE MIN. 3'-0" LANDING WHERE OCCURS	(HWH)	ON-DEMAND HOT WATER HEATER
				(HD)	HEAT DETECTOR/HEAT ALARM PER SRC R314.2.1



1 SECOND FLOOR PLAN
SCALE: 1/4" = 1'-0"

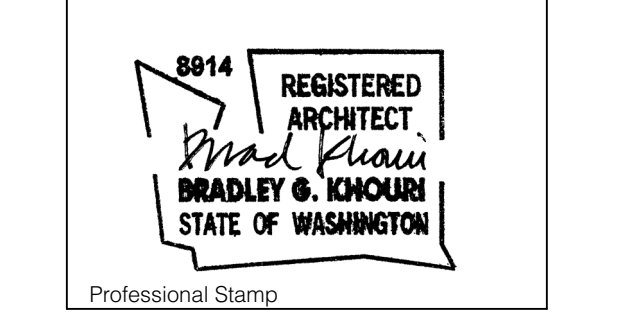


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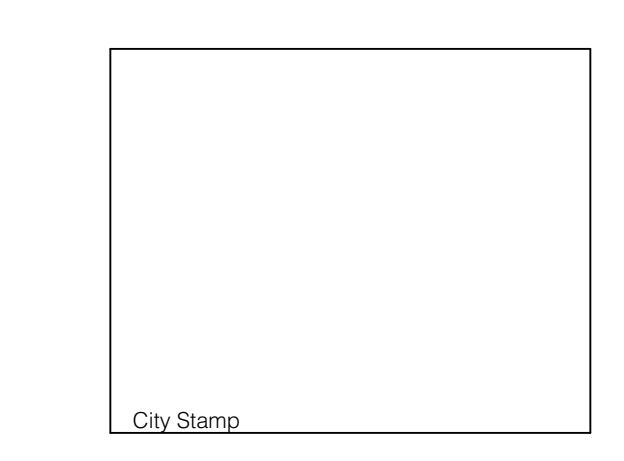
Project:
2740 61st Ave SE

Location:
2740 61ST AVE SE
MERCER ISLAND, WA 98040

SDCI Number:
#SDCI CN#



Issue ID	Issue Name	Issue Date



Second Floor Plan

A2.02



Shearwall Design Summary

M+K Project #: 300-24003

Engineer: MPM

Shearwall 201: 2nd - South Bedroom Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
 Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
 fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL plf Overturning Moment k-ft Hold Down Design Load lbs
 DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required

Shearwall 202: 2nd - South Bathroom Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
 Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
 fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL plf Overturning Moment k-ft Hold Down Design Load lbs
 DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required



Shearwall 203: 2nd - South Bedroom Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL plf Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required

Shearwall 204: 2nd - North Bedrooms Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL plf Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required



Shearwall 205: 2nd - Deck Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required

Shearwall 206: 2nd - Primary Bath Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required



Shearwall 207: 2nd - South Bedroom Rear Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required

Shearwall 208: 2nd - South Bedroom Front Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required



Shearwall Design Summary

M+K Project #: 300-24003
Engineer: MPM

Shearwall 209: 2nd - North Bedroom Front Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required

Shearwall 101: 1st - Garage South Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required



Shearwall Design Summary

M+K Project #: 300-24003
Engineer: MPM

Shearwall 102: 1st - Living Room South Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required

Shearwall 103: 1st - North Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required



Shearwall 104: 1st - Dining Rear Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P3 - 1-side 7/16" OSB
fastened w/ 8d nails at 3"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

SIMPSON STHD14RJ HOLDOWN

Shearwall 105: 1st - Dining Rear Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P3 - 1-side 7/16" OSB
fastened w/ 8d nails at 3"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

SIMPSON STHD14RJ HOLDOWN



Shearwall 106: 1st - Garage Rear Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required

Shearwall 107: 1st - Bath Front Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL pl f Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

SIMPSON STHD14RJ HOLDOWN



Shearwall 210: 2nd - Primary Bath Side Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL plf Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required

Shearwall 108: 1st - Outdoor Shed Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL plf Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

SIMPSON STHD14RJ HOLDOWN



Shearwall Design Summary

M+K Project #: 300-24003
Engineer: MPM

Shearwall 109: 1st - Outdoor Shed Ext Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL plf Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

SIMPSON STHD14RJ HOLDDOWN

Shearwall 110: 1st - Int. Garage Wall

Shearwall Properties:

Wall height, H ft. Max wall opening ht, H_c ft.
Wall Length, L ft. Qualifying Wall Length, L ft. Shearwall Assembly

Capacity Evaluation:

Total Shear Load on Wall lbs < Allowable Shearwall Capacity lbs

Shearwall Assembly Specification

P1 - 1-side 7/16" OSB
fastened w/ 8d nails at 6"o.c. panel edges & 12"o.c. panel field - edges blocked
ADEQUATE

Overturning Evaluation:

Resistive DL plf Overturning Moment k-ft Hold Down Design Load lbs
DL at ends of wall lbs Resistive Moment k-ft Hold down Capacity lbs

Hold-down Specification

No Hold down Required